

AD-A128 767

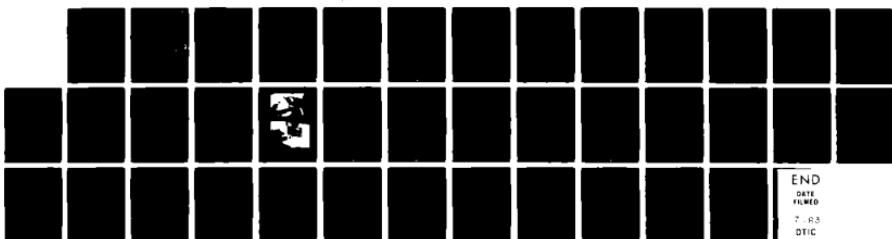
THERMAL CONDUCTIVITY OF WEATHERED POLYURETHANE FOAM  
ROOFING(U) NAVAL CIVIL ENGINEERING LAB PORT HUENEME CA  
D A ZARATE ET AL. SEP 82 NCEL-TN-1643

1/1

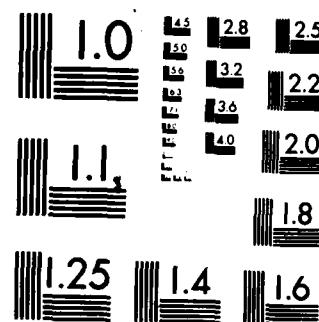
UNCLASSIFIED

F/G 13/1

NL



END  
DATE FILMED  
7-63  
DTIC



MICROCOPY RESOLUTION TEST CHART  
NATIONAL BUREAU OF STANDARDS 1963-A

ADA 128 767

TN NO: N-1643



**TITLE:** THERMAL CONDUCTIVITY OF WEATHERED  
POLYURETHANE FOAM ROOFING

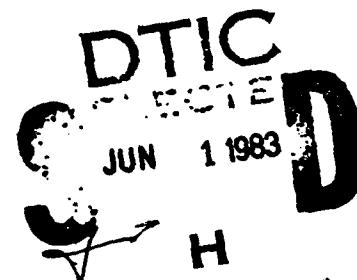
ADA 128 767

**AUTHOR:** D. A. Zarate and R. L. Alumbaugh, Ph D

**DATE:** September 1982

**SPONSOR:** Chief of Naval Material

**PROGRAM NO:** S0371-01-112B

DTIC  
RECEIVED  
JUN 1 1983  


**NOTE**

NAVAL CIVIL ENGINEERING LABORATORY  
PORT HUENEME, CALIFORNIA 93043

Approved for public release; distribution unlimited.

FILE COPY

DTIC

03 05 31 109

**METRIC CONVERSION FACTORS**

Approximate Conversions to Metric Measures		
Symbol	When You Know	Multiply by
<u>LENGTH</u>		
in	inches	2.5
ft	feet	30
yd	yards	0.9
mi	miles	1.6
<u>AREA</u>		
in <sup>2</sup>	square inches	0.65
ft <sup>2</sup>	square feet	0.09
yd <sup>2</sup>	square yards	0.8
mi <sup>2</sup>	square miles	2.6
acres	acres	0.4
<u>MASS (weight)</u>		
oz	ounces	28
lb	pounds	0.45
sh. tons	short tons (2,000 lb)	0.9
<u>VOLUME</u>		
sp	teaspoons	5
Tabp	tablespoons	15
fl oz	fluid ounces	30
c	cups	0.24
pt	pints	0.47
qt	quarts	0.95
gallons	gallons	3.8
cubic feet	cubic feet	0.03
cubic yards	cubic yards	0.76
<u>TEMPERATURE (excess)</u>		
°F	Fahrenheit temperature	5/9 (after subtracting 32)
<u>TEMPERATURE (exact)</u>		
°C	Celsius temperature	°C

Approximate Conversions from Metric Measures		
Symbol	When You Know	Multiply by
<u>LENGTH</u>		
in	millimeters	0.04
ft	centimeters	0.4
yd	meters	3.3
mi	feet	1.1
mi	yards	0.6
mi	miles	0.6
<u>AREA</u>		
in <sup>2</sup>	square centimeters	0.16
ft <sup>2</sup>	square meters	1.2
yd <sup>2</sup>	square kilometers	0.4
mi <sup>2</sup>	hectares (10,000 m <sup>2</sup> )	2.5
<u>MASS (weight)</u>		
oz	grams	0.035
lb	kilograms	2.2
sh. tons	tonnes (1,000 kg)	1.1
<u>VOLUME</u>		
fl oz	milliliters	0.03
pt	liters	2.1
Tabp	liters	1.06
fl oz	cubic meters	0.26
c	cubic meters	36
pt	cubic meters	1.3
<u>TEMPERATURE (exact)</u>		
°F	°Celsius temperature	9/5 (then add 32)
<u>TEMPERATURE (fahrenheit)</u>		
°C	°Fahrenheit temperature	5/9 (then subtract 32)

\*1 in = 2.54 (exactly). For other excess conversions and more detailed tables, see NBS  
Spec. Publ. 280, Units of Weights and Measures, Price 62-30, 50 Cents, Catalog No. C1310-280.

## Unclassified

SECURITY CLASSIFICATION OF THIS PAGE (When Data Entered)

REPORT DOCUMENTATION PAGE		READ INSTRUCTIONS BEFORE COMPLETING FORM
1. REPORT NUMBER <b>TN-1643</b>	2. GOVT ACCESSION NO. <b>DN987069</b>	3. RECIPIENT'S CATALOG NUMBER <b>AD-A128 767</b>
4. TITLE (and Subtitle) <b>THERMAL CONDUCTIVITY OF WEATHERED POLYURETHANE FOAM ROOFING</b>		5. TYPE OF REPORT & PERIOD COVERED <b>Final; Jan 1971 - Nov 1981</b>
7. AUTHOR(s) <b>D. A. Zarate and R. L. Alumbaugh, Ph D</b>		8. CONTRACT OR GRANT NUMBER(s)
9. PERFORMING ORGANIZATION NAME AND ADDRESS <b>NAVAL CIVIL ENGINEERING LABORATORY Port Hueneme, California 93043</b>		10. PROGRAM ELEMENT, PROJECT, TASK AREA & WORK UNIT NUMBERS <b>64710N; S0371-01-112B</b>
11. CONTROLLING OFFICE NAME AND ADDRESS <b>Chief of Naval Material Washington, DC 20360</b>		12. REPORT DATE <b>September 1982</b>
14. MONITORING AGENCY NAME & ADDRESS (if different from Controlling Office)		13. NUMBER OF PAGES <b>33</b>
		15. SECURITY CLASS. (of this report) <b>Unclassified</b>
		15a. DECLASSIFICATION/DOWNGRADING SCHEDULE
16. DISTRIBUTION STATEMENT (of this Report)  <b>Approved for public release; distribution unlimited.</b>		
17. DISTRIBUTION STATEMENT (of the abstract entered in Block 20, if different from Report)		
18. SUPPLEMENTARY NOTES		
19. KEY WORDS (Continue on reverse side if necessary and identify by block number)  <b>Roofs, energy conservation, insulation, polyurethane foam, thermal conductivity, thermal resistance.</b>		
20. ABSTRACT (Continue on reverse side if necessary, and identify by block number)  <b>An investigation of the decay in the thermal conductivity of polyurethane foam (PUF) with time is presented. The polyurethane foams studied included samples removed from sprayed PUF roofing systems on structures at Guam, Marianas Islands; Subic Bay, Republic of the Phillipines; Denver, Colorado; Clifton, New Jersey; and Port Hueneme, California. Thermal conductivity results closely agree with those predicted for a foam aged at 25°C in a controlled atmosphere. Results also indicate that the foam can provide good insulation characteristics in spite of poor application.</b>		

DD FORM 1 JAN 73 1473 EDITION OF 1 NOV 65 IS OBSOLETE

Unclassified

SECURITY CLASSIFICATION OF THIS PAGE (When Data Entered)

Unclassified

SECURITY CLASSIFICATION OF THIS PAGE(When Data Entered)

Library Card

Naval Civil Engineering Laboratory  
THERMAL CONDUCTIVITY OF WEATHERED POLY-  
URETHANE FOAM ROOFING (Final), by D. A. Zarate and  
R. L. Alumbaugh, Ph D  
TN-1643 33 pp illus September 1982 Unclassified

1. Energy conservation

2. Insulation

I. S0371-01-112B

An investigation of the decay in the thermal conductivity of polyurethane foam (PUF) with time is presented. The polyurethane foams studied included samples removed from sprayed PUF roofing systems on structures at Guam, Marianas Islands; Subic Bay, Republic of the Phillipines; Denver, Colorado; Clifton, New Jersey; and Port Hueneme, California. Thermal conductivity results closely agree with those predicted for a foam aged at 25°C in a controlled atmosphere. Results also indicate that the foam can provide good insulation characteristics in spite of poor application.

Unclassified

SECURITY CLASSIFICATION OF THIS PAGE(When Data Entered)

## CONTENTS

	Page
INTRODUCTION . . . . .	1
BACKGROUND . . . . .	1
SCOPE OF WORK . . . . .	2
EXPERIMENTAL . . . . .	3
RESULTS AND DISCUSSION . . . . .	3
FINDINGS AND CONCLUSIONS . . . . .	8
RECOMMENDATIONS . . . . .	9
ACKNOWLEDGEMENTS . . . . .	9
REFERENCES . . . . .	10
BIBLIOGRAPHY . . . . .	10

Accession For	
NTIS GENI	
DTIC TAB	
Unannounced	
Justification	
By	
Distribution/	
Availability Codes	
Avail	and/or
Dist	Special

A



## INTRODUCTION

Polyurethane foam (PUF) is produced by the spontaneous and exothermic reaction between a polyol and a polyisocyanate. The reacting components are foamed by the presence of a blowing agent, generally  $\text{CFC}_1_3$  (trichlorofluoromethane), which is vaporized by reaction exotherm. The installation of PUF as insulation in a sprayed PUF roof system is well-established, and its use is increasing. When properly formulated and applied, such a system has excellent weather (Ref 1, 2, and 3) and fire retardant properties (Ref 4, 5).

One of the primary reasons for the increasing use of PUF is its low thermal conductivity property which is one of the lowest available. Conversely, PUF's high thermal resistance is one of the highest available. Lining refrigerators almost exclusively with PUF further establishes PUF's credibility as an excellent insulating material.

When applied properly on roofs and protected with suitable elastomeric coatings, PUF roofing systems have excellent stability and weathering properties as well as low maintenance requirements. In the field, aging characteristics of the thermal conductivity have not been well established. Interest in this aspect is based on the increasing use of PUF roofing systems at Naval Shore Bases. The increased use of all types of insulation is based on the need to reduce overall consumption of energy. The aging characteristics of the thermal conductivity of PUF in such a roofing system is important in order to establish this material as a viable alternative to conventional insulation materials.

## BACKGROUND

The thermal conductivity ( $k$ ) of a material is a measure of the material's ability to transfer - or inhibit the transfer - of heat. The  $k$ -value is conventionally reported in  $\text{Btu}/(\text{hr})(\text{ft}^2)(^{\circ}\text{F}/\text{in.})$  and all values for  $k$  given in this report will be listed in these units. The better a material is able to inhibit the transfer of heat, the lower is its thermal conductivity or  $k$ -value. Note that the thermal conductivity is given for 1 inch of material. The insulating ability for materials of thicknesses other than 1 inch (usually greater than 1 inch) is the thermal resistivity or  $R$ . The thermal resistivity is the reciprocal of the thermal conductivity ( $1/k$ ) times the thickness: the higher the  $R$ -value, the better the insulation.

A literature survey revealed very little information on the thermal conductivity of sprayed PUF used in the construction industry. Some results were reported by European and Russian researchers, but these were not immediately available. Some excellent theoretical treatments and laboratory aging studies have been reported on the aging characteristics of thermal conductivity in PUF.

Norton (Ref 6) presented an excellent theoretical treatment of the change in thermal conductivity with time supported by some laboratory work. The change in thermal conductivity was addressed by considering the thermal conductivities of individual components (CFC<sub>13</sub>, polymer, air) and the diffusion coefficients of the gases through the polymer (PUF). While this work was directed toward the use of PUF in refrigeration, its use as insulation is equally pertinent to foam in PUF roofing systems.

Using 2.2 pcf (pounds-per-cubic foot) density foam with all cells filled with CFC<sub>13</sub>, the experimentally determined k-value was 0.100 (6).

The thermal conductivity contribution of CFC<sub>13</sub> is 0.057 at 1 atmosphere and 25°C. Subtracting 0.057 from the k-value determined for PUF (0.100) gives the polymer contribution as 0.043. Taking the polymer contribution and adding it to the thermal conductivity for air (0.176) suggests that the maximum attainable k-value for this foam is 0.219. This latter value assumes complete displacement of CFC<sub>13</sub> by air but no intrusion of water or water vapor.

From experimental data and application of Fick's law for diffusion of matter in solids and the Fourier equation upon which Fick's law is based, Norton in Reference 6 determined the diffusion constants for CFC<sub>13</sub>, nitrogen, and oxygen to be  $2.25 \times 10^{-9}$ ,  $6.27 \times 10^{-8}$  and  $1.12 \times 10^{-7}$  cm<sup>2</sup>/sec, respectively.

With these values, Norton predicted that it would require 50 years for a 12x12x1-inch PUF sample to reach its maximum (air-filled only) thermal conductivity and 200 years for a 12x12x2-inch PUF sample to reach its maximum. At 50 years, the predicted k-value for the 2-inch-thick PUF is 0.19. These predictions were for a 2.2-pcf-density PUF, 12x12 inches and 1 or 2 inches thick, all sides exposed to the air at 25°C (77°F) and without the intrusion of water or water vapor.

In Reference 7, Ball, Hurd, and Walker compared existing and new aging data with Norton's theoretical treatment of the change in thermal conductivity with time. The experimental results agreed remarkably well with the theoretical. Based on their experiments, Ball et al. also predicted that the maximum thermal conductivity of the PUF aged at room temperature would be achieved after approximately 100 to 200 years. It should be emphasized that all of the predicted values are based on aging under ambient laboratory conditions with no consideration given to the effects of exposure to exterior weather conditions.

## SCOPE OF WORK

The objective of this work was to evaluate samples of sprayed PUF roofing systems that had been exposed to various climatic conditions for varying periods of time. Particular emphasis was placed on obtaining roof samples that were 5 or more years of age. This was done in order to collect data on the thermal conductivity of materials that have undergone long-term aging under actual field conditions. The disadvantage of such an approach is that it is not always possible to obtain all pertinent data such as coating or foam types, manufacturer, installation date, or conditions. In spite of this, sufficient data were generally obtained on each sample to make the thermal conductivity data useful.

Aged PUF roof samples were obtained from roofs at: (1) the Naval Reserve Center, Clifton, New Jersey; (2) the U. S. Bureau of Reclamation, Denver, Colorado (one sample from a roof; other samples were from foam roofing that had been sprayed on concrete panels cast on the ground); (3) Naval Station, Guam, Marianas Islands; (4) Naval Base, Subic Bay, Republic of the Philippines; and (5) Naval Civil Engineering Laboratory (NCEL), Port Hueneme, California. In each case, an attempt was made to obtain samples at least 1 foot square in size (Figure 1). However, on occasion, the adhesion of the PUF to the roof deck was so great that it was not possible to obtain this size without some breakage. Once the sample was cut and pried from the roof, it was wrapped in a plastic bag to prevent any loss or gain of moisture, if present, and shipped to NCEL for testing. The samples ranged in age from 1 to 11 years.

## EXPERIMENTAL

Once the samples were received at NCEL, they were prepared for testing and their thermal conductivity determined as soon as possible. Sample preparation consisted of squaring the edges and top and bottom surfaces with a band saw. It was necessary to have the top and bottom surfaces flat and parallel. A belt sander was used to achieve this requirement after cutting. The thermal conductivity of the prepared samples was determined using a thermal conductivity analyzer, Model 88 from Anacon, Inc. (Figure 2). Each time k-values were determined, the Model 88 was calibrated using a National Bureau of Standards fiberglass insulation standard. The Model 88 accepts samples from 4 x 4 inches to 8 x 8 in., square or rectangular, and 0.62 to 2.20 inches thick. By definition, the k-value is for a sample 1 inch thick, and the Model 88 automatically determines the k-value for a 1 inch thick sample.

## RESULTS AND DISCUSSION

Test results are presented in Table 1 and are grouped according to geographical location. The sprayed foam roof samples tested were coated with various generic types of coating systems. In addition, part of the coating systems were permeable or "breathing." Permeable coatings allow more rapid diffusion of water vapor or air through the coating system. Impermeable coatings are vapor retarders which, as the name implies, may severely retard but do not prevent the diffusion of water vapor or air through the coating.

Permeability of coatings is generally determined in accordance with ASTM standard method E-96. The unit of permeability (or permeance) is 1 perm-inch (or 1 perm) which is equivalent to 1 gr/hr x ft<sup>2</sup> inches of mercury inches of thickness (or 1 perm is equivalent to 1 gr/hr x ft<sup>2</sup> inches of mercury). Within the industry, an arbitrary cutoff point has been established as 1 perm. With this arbitrary standard, coating systems having a perm rating >1 are considered permeable while those with perm ratings <1 are considered impermeable.

The first set of results listed in Table 1 are for samples obtained from the Clifton, New Jersey, test site. These roofs were sprayed in October 1973, and the samples taken in October 1978. All of these are CPR Upjohn's #485-2 PUF, 2-pound density, with good small cell structure.

The lowest two readings are from foams coated with a permeable over an impermeable coating. These samples - 4b and 5a - have a total coating thickness of 45 mils ( $k = 0.139$ ) and 10 mils ( $k = 0.138$ ), respectively.

The highest three samples are 2a, 2b, and 1a and are coated with permeable coatings. For 2a, 2b, and 1a, respectively, the total coating thicknesses are 7 mils ( $k = 0.172$ ), 20 mils ( $k = 0.176$ ), and 20 mils ( $k = 0.178$ ).

Except for 3a, all foam samples from this area that were coated with an impermeable coating have lower, therefore, better  $k$ -values than those coated with a permeable coating. All of the samples are 5 years old and were approximately 2 inches thick on the roof. The predicted 5-year  $k$ -value for a 2.2-pcf-density PUF, 12 x 12 x 2-inch slab, aged at 25°C (77°F) is 0.148 (Ref 6). From Table 2, the overall average  $k$ -value of these samples is 0.158 which is closer to the predicted  $k$ -value of 0.158 for a 12 x 12 x 1-inch slab. However, the  $k$ -value for the samples with an impermeable coating averages 0.146, and those with a permeable coating average 0.170. This shows a strong correlation between samples with impermeable coatings aged at Clifton, New Jersey, and samples without coatings aged under controlled laboratory conditions.

The perm ratings of permeable coatings (2 to 3 perms) is close to, or equivalent to, that of PUF (approximately 2 perms). A permeable coating allows the foam to breathe and release excessive water vapor. Impermeable coatings (perm ratings  $<1$ ) retard the entrance or release of excessive water vapor and to some extent retard the passage of air as well. Excessive moisture could also be liquid water that has intruded through breaks in the coating. Water vapor or air, once past the coating, would diffuse at a faster rate into the foam (low concentration of air and water) rather than back out into the atmosphere (high concentration of air and water). The diffusion rate could be increased by the presence of a strong "moisture drive."

A moisture drive exists when there are warm temperatures and high humidity on one side of a partition or roof and cooler temperatures with lower humidity on the other. This effectively "drives" or forces moisture from the warmer side to the cooler side in an effort to equilibrate. Moisture drives exist in areas such as the South Pacific and Eastern Seaboard where buildings are generally air conditioned during warm weather.

The climatic conditions in Clifton can vary from around 38°C (100°F) and 70% relative humidity to 10°C (50°F) and 50% relative humidity daily in the summer and from around 18°C (65°F) and 70% relative humidity to -18°C (0°F) and 50% relative humidity daily in the winter.

Because of the moisture drive in this area, permeable coatings would allow the  $k$ -value of PUF to increase at a greater rate than those with impermeable coatings. Due to the greater rate at which water vapor and air pass through the permeable coating, the  $k$ -value of the PUF would tend to increase more rapidly than with an impermeable coating and results bear this out.

In areas with a moisture drive, results indicate that an impermeable coating may help keep the  $k$ -value from increasing faster than that found under controlled laboratory conditions. Results also show that, in spite of the harsher conditions found at Clifton, the  $k$ -values of PUF with impermeable coatings agree very well with those predicted for PUF aged at 25°C under controlled atmospheric conditions.

The next set of results listed in Table 1 is for samples of Systems 6 through 12 and was obtained from the Denver, Colorado, test site. Sample 12 was sprayed on a roof deck while the rest were sprayed over concrete panels located on the ground; Samples 6 and 7 are about 10-1/2 years old and have a good small cell structure. Samples 8 and 9 are almost 10 years old (9-3/4) and in general show a good small cell structure; Sample 8 appears to have been exposed for a few days before being coated (the coating easily peeled off and the surface was sun burnt) while Sample 9 has a 1/4-inch-deep gouge in the center of the sample. Samples 10 and 11 are about 4 years old (4-1/3) with a rather coarse and large cell structure. At least 50% of the cells are larger than a pinhead and perhaps 10% to 20% are twice that size with a small percentage (less than 10%) of small cells. Sample 12 is about 6-1/2 years old with about 10% large cells and more than 50% small cells.

The two lowest thermal conductivity readings are from Samples 8 and 9; Sample 8 ( $k = 0.170$ ) was coated with 15 mils of a permeable coating and Sample 9 ( $k = 0.169$ ) was coated with 7 mils of an impermeable coating. Both are almost 10 years old. Sample 9 has an extremely irregular surface with the coating degrading and exposing the foam. If a coating, especially an impermeable one, is to be effective, it must cover the foam surface entirely and be applied at the proper thickness; 7 mils is only about one-third the minimum acceptable thickness. This and the gouge in the surface of Sample 9 may explain the similar  $k$ -values of Samples 8 and 9.

The  $k$ -values of the rest of the samples range from approximately 0.19 to 0.20. The disparity of these values with the age of the samples may be explained by the lack of proper thickness in the coatings, by larger cell structures, and by the fact that the concrete slab on which the foam was applied was directly on the ground. This may have contributed to more rapid diffusion of moisture vapor into the foam. In comparing the foam characteristics and the  $k$ -value of Sample 9 to that of Samples 10, 11, and 12, the only apparent difference that could make the  $k$ -value of Sample 9 lower is the cell structure. The difference is even more apparent when Sample 8 is compared with Sample 9.

The next set of results listed in Table 1 was obtained from roof samples at Subic Bay in the Philippines and from Guam. These samples illustrate some adverse effects on PUF roofs caused by poor application of either the PUF, the coatings, or both.

The first three samples (13 to 15, which had  $k$ -values = 0.18 to 0.19) were coated with an exterior house paint, not a coating formulated for protecting PUF or even for use on roofs. The samples are about 6 years old. They show signs of severe checking and cracking with about 10% to 20% of the coating flaking from the foam surface; the paint is also very brittle. Samples 13 and 15 appear to have been applied over a wet surface as indicated by the poor quality of foam surface adjacent to the deck.

Sample 16 was coated with 10 mils of a permeable coating and is approximately 4 years old. The bottom of the foam adjacent to the roof deck was wet, and the coating was alligatoring in low spots but was continuous over a rough foam surface. The coating was, therefore, still protecting the foam from the sun and intrusion of water; the  $k$ -value of the foam was about 0.16.

Sample 17 was in good condition and was about 5 years old. It has the same coating as on Sample 16; the foam has a  $k$ -value of 0.17.

Internally, beyond both surfaces, these samples had a good cellular structure. This may have been fortuitous since all of the k-values are less than 0.20. These roofs will probably continue to render fairly good insulating service.

Sample 18 from Guam is coated with an asphalt-based coating of unknown permeability. The system was about 5 years of age with a badly deteriorated surface and some patching of the coating.

Sample 19 from Guam was taken from a PUF roof that had been maintained, (i.e., a second layer of foam was sprayed over an existing PUF roof in which both the coating and the foam had degraded). The original coating over the foam was a paint (not meant for roof surfacing) while the second layer or new foam had a permeable silicone coating. No k-value could be determined for the first (bottom) foam layer because of its small size. The second layer had a value of nearly 0.26. This higher k-value may have been due in part to entrapped moisture in the first layer migrating into the second. However, the most significant cause for this higher k-value may be the poor foam cell structure. Approximately 50% of the sample had large (1/8 to 1/2 inch across) cell voids while the remainder had normal, uniform, small cells.

Sample 20a from Guam was 10 years old, had a good cell structure, and a reasonably good k-value. The surface had been maintained with a second coating applied after the original coating had degraded somewhat.

The last set of results listed in Table 1 are for samples obtained from roofs at NCEL, Port Hueneme, California. All of the buildings are unnorth and south except for a flat roof where Sample 29a was taken. All samples were cut in July 1981. For ease of discussion, the samples are relisted in Table 3 in order of increasing k-value.

Considering Samples 21b, 21a<sub>1</sub>, and 21a<sub>2</sub>, 28b, and 28a as 5-year-old samples, the overall average k-value is  $0.139 \pm 0.010$  and the average thickness is  $2.20 \pm 0.21$  inches. The average k-value of the two 2-inch samples is  $0.146 \pm 0.013$ . Reference 6 indicated that the 5-year predicted k-value for a 2.2 pcf density foam, 12 x 12 x 2 inches, aged under controlled conditions is 0.148. The experimental results agree very well with the predicted values (see Tables 4 and 5).

All the 7-year-old samples with impermeable coatings have an average k-value and thickness of 0.159 and 1.75 inches, respectively; with permeable coatings it is 0.170 and 1.69 inches respectively. Overall it is 0.164 and 1.72 inches, respectively.

Interpolating the 5- and 10- year predicted k-values to a 7-year sample, the k-values are 0.165 and 0.150 for a 1- and a 2-inch-thick 12x12-inch slab, respectively (Ref 6). The overall average k-value for the 7-year samples ( $k = 0.164 \pm 0.020$ ) at NCEL agrees more closely with the predicted 1-inch-thick sample value. The samples with an impermeable coating are only slightly lower ( $k = 0.159 \pm 0.018$ ). Taking only the 2-inch-thick 7-year-old-samples into consideration, the average k-value for samples with an impermeable coating is  $0.144 \pm 0.004$ , and for those with a permeable coating the k-value is  $0.148 \pm 0.012$ . These latter values agree very well with the predicted value of 0.150 for a 2 inch thick sample and indicate that thickness plays a significant role in the thermal conductivity aging characteristics of PUF.

The climatic conditions at NCEL can vary from about 35°C (95°F) to 7°C (45°F) daily in the summer and from around 25°C (77°F) to 1°C (34°F) in the winter. The average relative humidity percentage remains fairly

constant at approximately 70% due to the proximity of the ocean. The relative humidity percentage can vary from a low of about 60% to a high of about 80%. Lows of 15% to 20% relative humidity are infrequent and occur on days when hot, dry winds blow through the area.

The basic function of all coatings used on PUF is to protect the foam from sunlight (especially ultraviolet light), moisture, and consequent degradation. The permeable and impermeable coatings are rated on their ability to keep water vapor from passing through the coating film.

The k-value of water vapor at 25°C (77°F) and 1 atmosphere is 0.123, and for liquid water is 4.20.\* The k-value at the same conditions for air is 0.176, that for  $\text{CFC}_1_3$  is 0.057, and polymer can be taken to be 0.043 to 0.061 for a foam 2.0 to 3.0-lb/cu ft density respectively. With these values it is seen that foam filled with air (theoretical maximum k-value = 0.219 to 0.237) will have a higher k-value than if filled with water vapor only (theoretical maximum k-value = 0.166 to 0.184). In areas where a moisture drive might exist, results indicate that an impermeable coating may be better than a permeable coating.

At NCEL Port Hueneme, there is no strong evidence to indicate that impermeable coatings are much better than permeable coatings in keeping the k-value of PUF low with aging. Also, the climatic conditions at Port Hueneme are not as harsh or as severe as those found at Clifton. This suggests that the permeability of the coatings may not be a significant factor in the aging of thermal conductivity in PUF in areas such as Port Hueneme or where a moisture drive might not exist or be very strong.

Since the k-values of aged samples are fairly close to predicted values, this implies a predictability of the thermal conductivity of PUF in spite of varying temperatures and climates.

In Table 6 all samples are listed according to increasing k-value. With one exception, all samples had k-values  $< 0.20$ . The exception was a poor quality foam exhibiting large voids in the cellular structure. In Table 2, the average for all samples is shown to be  $0.163 \pm 0.022$ . In Reference 9 a k-value equal to 0.16 has been established as a design value for a 1.5 pcf density PUF. The experimental values given in this report provide a firm basis for the use of 0.16 as a design k-value for 2.0 to 3.0 lb/cu ft density PUF. The experimental values also show that, even though the k-value does decay, PUF remains equal to or better than the next best material, extruded Styrofoam, which maintains a k-value of 0.20 (Ref 10).

The overall PUF and coating quality was found to be best in the NCEL and Clifton samples, followed by the Denver samples and, finally, the Guam and Subic Bay samples. From the standpoint of temperature fluctuations, the harshest environments would be those found at Clifton and Denver followed by NCEL, then Guam and Subic Bay.

A point borne out by Table 6 is that all samples below  $k = 0.164$ , except for one from Subic Bay, are from NCEL or Clifton. This may in part be due to the better foam quality and in part to the samples being cut from PUF sprayed on roofs rather than on panels as at Denver.

---

\*Interpolated and converted from  $\text{Cal}/(\text{sec})(\text{cm}^2)(^\circ\text{C}/\text{cm})$  values given in Reference 8 by dividing by  $3.445 \times 10^{-4}$ . The conversion factor given in Reference 6 can also be multiplied by the conversion factor given in Reference 8 if results are also multiplied by 12 to convert from  $^\circ\text{F}/\text{ft}$  to  $^\circ\text{F}/\text{in.}$

It is also noticed that most of the samples below 0.164 from Clifton have an impermeable coating. Comparing the averages of the samples from NCEL and Clifton in Table 2, the samples with permeable coatings from NCEL ( $k = 0.153$ ) have a significantly better  $k$ -value than those from Clifton ( $k = 0.170$ ). The samples with impermeable coatings are about the same when age is considered and when compared to the predicted values (Ref 6) for a PUF aged at  $25^\circ\text{C}$  ( $77^\circ\text{F}$ ). This indicates that impermeable coatings help to maintain a low thermal conductivity in PUF and even keep the aging to a point similar to that where the permeability of the coating does not play a significant role. Comparison of the NCEL and Clifton averages suggests again that impermeable coatings may be better than permeable coatings where a moisture drive exists; in other areas where a strong moisture drive does not exist, they may not exhibit a significant effect on the aging of the thermal conductivity. Figure 3 compares graphically the  $k$ -values reported here according to age and coating type (permeable or impermeable).

A comparison of the averages of the Clifton and the 7-year-old NCEL samples to those predicted values in Reference 6 show good agreement between those samples with impermeable coatings and the 2-inch-thick predicted samples. This suggests that the  $k$ -value for PUF roofing systems in the field may be predicted for those with impermeable coatings. For PUF roofing systems with permeable coatings in areas such as Clifton,  $k$ -values may be predicted by adding 0.03 to those predicted for PUF with impermeable coatings. In areas such as NCEL Port Hueneme, predicted  $k$ -values for systems with impermeable coatings may be used for systems with permeable coatings.

This predictability implies that varying climatic conditions may not be significant if the PUF is properly coated with an impermeable coating. This is in spite of the large daily and yearly changes in temperature, humidity, rain, snow, or other weather conditions to which the PUF roofing systems may be subjected.

Factors not specifically considered which may play a part in the thermal conductivity aging characteristics are foam thickness, percentage of open cells, cell structure and size, foam density, cell orientation, and surface skins.

#### FINDINGS AND CONCLUSIONS

The following findings and conclusions are presented on the basis of the data contained in the report on the thermal conductivity of PUF roofing specimens aged from 1 to 10-1/2 years.

1. Impermeable coatings help to maintain a low thermal conductivity factor in PUF better than permeable coatings. In areas where a strong moisture drive exists, this becomes even more pronounced. In areas where a moisture drive does not exist or is weak, the effect on aging by the type of coating used appears insignificant.

2. Good agreement exists between PUF samples aged in the field under harsh climatic conditions with an impermeable coating and predicted k-values for PUF samples with no coating aged in the laboratory at 25°C (77°F) under controlled atmospheric conditions. This implies a predictability to the life of a PUF system in the field if the foam and coating are properly applied and maintained.

Another major factor in maintaining a low thermal conductivity with time is the thickness; i.e., the thicker the PUF, the longer it takes for the thermal conductivity to increase. This is also noted in the predicted values for 2-inch and 1-inch-thick 12x12-inch slabs Reference 6. The predicted time for the 2-inch-thick sample to reach its theoretical maximum is approximately 200 years, and for the 1-inch-thick sample it is approximately 50 years. Even though the 2-inch sample is only twice as thick as the 1-inch sample, it may require four times as long to achieve its maximum. This is, of course, theoretical at this time.

3. A k-value of 0.16 may be established as a design value for 2.0- to 3.0-pcf-density PUF.

4. In spite of poor application and maintenance, it has been shown that a PUF roofing system can still provide good service with respect to k-value decay. However, such decay occurs more rapidly with foam roof systems that are improperly applied and maintained, than with those that are properly applied and maintained.

5. In spite of the decay in k-value, PUF is equal to or better than the next best material (extruded Styrofoam<sup>®</sup>) for maintaining a low k-value.

#### RECOMMENDATIONS

1. Polyurethane foam should be applied to achieve a uniform small cell structure and as smooth a surface texture as possible in order to obtain the best thermal conductivity properties.

2. A coating should be used that has been formulated for protecting PUF from the sunlight and weather. Where a significant moisture drive exists, an impermeable coating is recommended.

3. Protective coatings should be applied to their proper minimum film thickness (generally manufacturer's recommended thickness). A thin coating thickness may result in premature exposure of the foam to the sun and degradation and the possible intrusion of water.

4. In harsh environments it is even more important to maintain the coating in the PUF system at the proper minimum film thickness.

#### ACKNOWLEDGMENTS

The authors wish to express their appreciation to Ms. Nathalie Milliken and Mr. Valente Hernandez for sampling the roofs at NCEL; to Mr. Bernard V. Jones, U.S. Bureau of Reclamation, Denver, Colorado, for

supplying the samples from the Denver site; to Mr. Charles Schembri, U.S. Navy Public Works Center, Subic Bay, R. P., for sending samples; and to the Navy Public Works Center, Guam, Marianas Islands, for supplying samples.

#### REFERENCES

1. Civil Engineering Laboratory. Technical Note N-1450: Experimental polyurethane foam roofing systems, by J. R. Keeton, R. L. Alumbaugh, Ph.D., and E. F. Hamm. Port Hueneme, Calif., Aug 1976.
2. . Purchase Order No. 79-MR-461: Principles of urethane foam roof application, by Keith H. Coultrap. Tempe, Ariz., Coultrap Consulting Services, Inc., Jun 1980.
3. . Technical Note TN No. N-1496: Investigation of spray-applied polyurethane foam roofing systems-I, by R. L. Alumbaugh, Ph.D. and J. R. Keeton, P.E. Port Hueneme, Calif., Jul 1977.
4. Underwriter's Laboratories, Inc. Building Materials Directory. Chicago, Ill., Jan 1981, pp 480-482.
5. Civil Engineering Laboratory. Contract Report CR 79.004: Fire tests of polyurethane foam roof deck construction on steel decks. Chicago, Ill., Underwriter's Laboratories, Dec 1978.
6. Francis J. Norton. "Thermal conductivity and life of polymer foams," Journal of Cellular Plastics, vol 3, no. 1, 1967, pp 23-37.
7. G. W. Ball, R. Hurd, and M. G. Walker. "Thermal conductivity of rigid urethane foams," Journal of Cellular Plastics, vol 6, no. 2, 1970, pp 66-78.
8. Chemical Rubber Company. CRC Handbook of Chemistry and Physics, 49th Edition. Cleveland, Ohio, 1968-1969, pp E-2 to E-4.
9. ASHRAE Handbook of Fundamentals. New York, N.Y., American Society of Heating, Refrigeration and Air Conditioning Engineers, Inc., 1977.
10. Civil Engineering Laboratory. Contract Report CR 80.001: Building insulation materials compilation. Cambridge, Mass., Dynatech R/D Co., Jan 1980.

#### BIBLIOGRAPHY

Brandreth, D. A. and H. G. Ingersoll (1980). Accelerated aging of rigid polyurethane foam, Journal of Cellular Plastics, vol 16, no. 4, 1980, pp 235-238.

Traeger, Richard K. (1967). "Physical properties of rigid polyurethane foams," Journal of Cellular Plastics, vol 3, no. 9, 1967, pp 405-18.

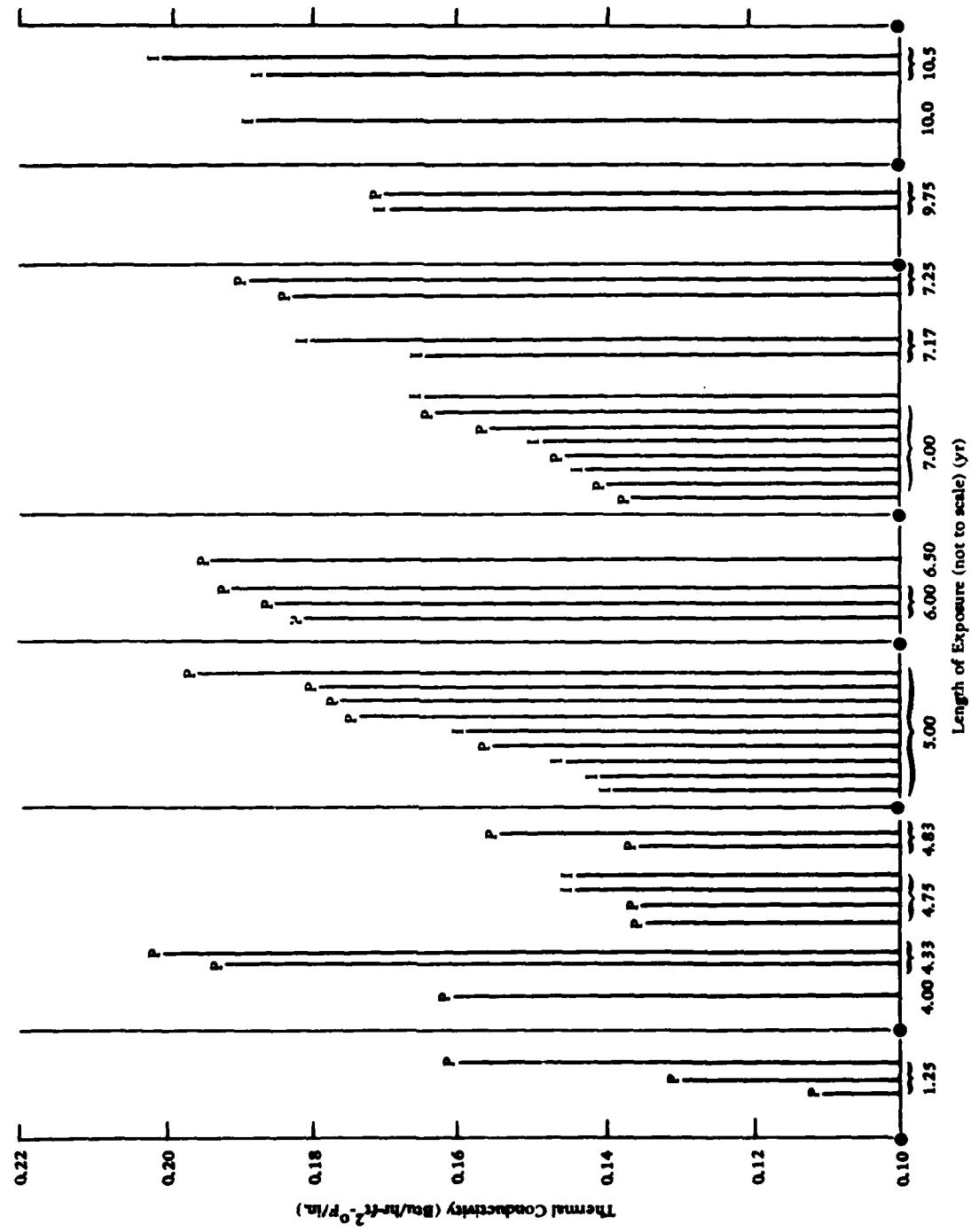
Vailand, Robert H. (1966). "Long-term k-factor aging of rigid urethane foam insulation," Journal, American Society of Heating, Refrigeration, Air-conditioning Engineers (ASHRAE), vol 8, no. 10, 1966, pp 84-89.



Figure 1. Taking a PUF sample from a roof.



Figure 2. Determining thermal conductivity on the Model 88 Thermal Conductivity Analyzer from Anacon, Inc.



**Figure 3.** Comparison of retained k-value on the basis of coating type (permeable versus impermeable).

Table 1. Thermal Conductivity (k) of Polyurethane Foam Samples From Weathered PUF Roof Systems

Sample No.	Coating/Foam System	Roof/Foam Description	Age (yr)	Foam Density (pcf) and Quality	Coating Thickness (mils) <sup>b</sup>			Foam Thickness (in.)	Thermal Conductivity (Btu/hr-ft <sup>2</sup> -°F/in.)	Comments
					First Coat	Second Coat	Third Coat			
Samples from Clifton Test Roofs <sup>c</sup>										
1a <sub>1</sub>	General Electric Silicone with Granules/CPR Upjohn 480-2.0	5	2.0/good, uniform cell structure	10 (P)	10 (P)	-- (P)	20 (P)	2.0	1.32	0.181
1a <sub>2</sub>		5	2.0/good, uniform cell structure	10 (P)	10 (P)	-- (P)	20 (P)	2.0	1.46	0.175
1b <sub>1</sub>	General Electric Silicone w/o Granules/CPR Upjohn 480-2.0	5	2.0/good, uniform cell structure	15 (P)	5 (P)	-- (P)	20 (P)	2.0	1.37	0.156
1b <sub>2</sub>		5	2.0/good, uniform cell structure	15 (P)	5 (P)	-- (P)	20 (P)	2.0	1.35	0.156
2a <sub>1</sub>	Dow Corning Silicone/CPR Upjohn 480-2.0	5	2.0/good, uniform cell structure	7 (P)	-- (P)	-- (P)	7 (P)	1.75	1.09	0.181
2a <sub>2</sub>		5	2.0/good, uniform cell structure	7 (P)	-- (P)	-- (P)	7 (P)	1.75	1.09	0.169
2b <sub>1</sub>	Dow Corning Silicone/CPR Upjohn 480-2.0	5	2.0/good, uniform cell structure	10 (P)	10 (P)	-- (P)	20 (P)	2.25	1.57	0.188
2b <sub>2</sub>		5	2.0/good, uniform cell structures	10 (P)	10 (P)	-- (P)	20 (P)	2.25	1.58	0.171
3a <sub>1</sub>	U.S. Polymeric Butyl-Hypalon base + Dow Corning Silicone w/granules topcoat/CPR Upjohn 480-2.0	5	2.0/good, uniform cell structure	10 (I)	-- (I)	5 (I)	15 (I)	2.25	1.42	0.160
3a <sub>2</sub>		5	2.0/good, uniform cell structure	10 (I)	-- (I)	5 (P)	15 (I)	2.25	1.58	0.155

continued

Table 1. Continued

Sample No.	Roof Coating/Foam System Description	Age (yr)	Foam Density (pcf) and Quality	Coating Thickness (mils) <sup>b</sup>			Foam Thickness (in.)	Thermal Conductivity (Btu/hr-ft <sup>2</sup> -°F/in.)	Comments	
				First Coat	Second Coat	Third Coat	Total	Roof (Avg)		
4a <sub>1</sub>	Monolair Mastic Base + Carboline Rooflex 145/155 topcoat/CPR Upjohn 480-2-0	5	2.0/good, uniform cell structure	15 (1)	20 (P)	20 (P)	55 (1)	2.0	1.37	0.148
4a <sub>2</sub>		5	2.0/good, uniform cell structure	15 (1)	20 (P)	20 (P)	55 (1)	2.0	1.37	0.146
4b <sub>1</sub>	Monolair Mastic Base + Carboline Rooflex 145/155 topcoat/CPR Upjohn 480-2-0	5	2.0/good, uniform cell structure	20 (1)	10 (P)	15 (P)	45 (1)	2.25	1.50	0.143
4b <sub>2</sub>		5	2.0/good, uniform cell structure	20 (1)	10 (P)	15 (P)	45 (1)	2.25	1.48	0.135
5a <sub>1</sub>	United Coatings Butyl-Hypalon Base + Iirathane 300/394 w/granules/CPR Upjohn 480-2-0	5	2.0/good, uniform cell structure	5 (1)	--	10 (P)	15 (1)	2.25	1.51	0.144
5a <sub>2</sub>		5	2.0/good, uniform cell structure	5 (1)	--	10 (P)	15 (1)	2.25	1.48	0.137
Samples from U.S. Bureau of Reclamation, Denver, Colorado										
6	General Electric Siliccone/PPG Foam	10-1/2	2.0/good, uniform cell structure	12 (P)	--	--	12 (P)	1.50	1.12	0.202
7	United Butyl-Hypalon/PPG Foam	10-1/2	2.0/good, uniform cell structure	3 (1)	--	--	3 (1)	1.50	1.08	0.191
8	Dow Corning Silicone/North American Foam	9-3/4	2.0/good cell structure, irregular surfaces, top sunburnt	15 (P)	--	--	15 (P)	2.00	1.57	0.170

continued

Table 1. Continued

Sample No.	Roof Coating/Foam Description System	Age (yr)	Foam Density (pcf) and Quality	Coating Thickness (mils) <sup>b</sup>			Foam Thickness (in.)	Thermal Conductivity (Btu/hr-ft <sup>2</sup> -°F/in.)	Comments	
				First Coat	Second Coat	Third Coat	Total	Roof (Avg)		
9	Gaco-SBR base Hypalon topcoat/North American Foam	9-3/4	2.0/good cell structure, some larger holes (~10%)	2 (1)	5 (1)	--	7 (1)	1.50	0.169	Coating thin because of chalking and erosion. Extremely irregular surface, coating cratered and foam exposed.
10	Dow Corning Silicone/United Foam	4-1/3	2.0/good, uniform cell structure	10 (P)	10 (P)	--	20 (P)	2.00	0.189	
11	Carboline Rooflex/United Foam	4-1/3	2.0/good, uniform cell structure, ~10% medium holes	150 (P)	20 (P)	5 (P)	175 (P)	2.00	0.198	Coating excessively thick
12	General Electric Siliccone/Vitco Foam	6-1/2	2.0/good, uniform cell structure	10 (P)	10 (P)	--	20 (P)	2.25	0.194	Sample from roof deck
Samples from U.S. Naval Base, Subic Bay, R.P.										
13	TT-P-19 Latex paint/foam type unknown)	6	unknown/foam quality fair, irregular cell structure: 10%-20% large cells	15 (P)	--	--	15 (P)	1.25	0.186	Coating checking, cracking and flaking. Approximately 10% flaked off. Coating brittle. Sample from Ship Repair Facility (SRF) roof.
14	TT-P-19 Latex paint/foam type unknown)	6	unknown, fairly uniform cell structure ~10% large cells	15 (P)	--	--	15 (P)	1.25	0.182	Coating checking, cracking and flaking severely. Sample from Ship Repair Facility (SRF) roof.
15	TT-P-19 Latex paint/foam type unknown)	6	unknown, fair cell structure, foam applied over wet surface 20%-30% large cells	--	--	--	1.75 (P)	1.26	0.189	Coating badly deteriorated. Appears to have aluminum asphalt patch over poor coating. No coating thickness determined. Irregular sample from SRF roof.
16a <sub>1</sub>	Gaco A-5600 acrylic/Foam Systems FSC 26 Foam	4	2.0/good, uniform cell structure. Foam wet on one surface corner	10 (P)	--	--	10 (P)	2.00	0.168	Coating applied over rough surface and is alligatoring in low spots. Coating is continuous.
16a <sub>2</sub>		4		10 (P)	--	--	10 (P)	1.62	0.154	

continued

Table 1. Continued

Sample No.	Roof Coating/Foam System Description	Age (yr)	Foam Density (pcf) and Quality	Coating Thickness (mils) <sup>b</sup>			Foil Thickness (in.)	Thermal Conductivity (Btu/hr-ft <sup>2</sup> -°F/in.)	Comments		
				First Coat	Second Coat	Third Coat					
17	Gaco A-5400 acrylic / Foam Systems FSC 26 Foam	5	2.0/good, uniform cell structure. Foam dry	15 (P)	--	--	15 (P)	1.5	1.06	0.173	Coating in good condition.
Samples from U.S. Naval Station, Guam, M.I.											
18	Uniflex Aluminum/CPR Upjohn 425 foam	5	2.0/fair cell structure and uniformity	5 (P)	--	--	5 (P)	1.25	0.66	0.195	Badly deteriorated coat- ing - some patching.
19	Dow Corning w/granules over Witco Foam over PPG 19/PPG Foam	4-1/3	2.0/3.0; 50% fair cell structure, the rest composed of large open areas from 1/8" to 1" across	12 (P)	--	--	12 (P)	1.00	0.56	0.259	PPG Foam not run sample too small. TI-P-19 PPG Foam surface degraded. Values are for Witco foam layer.
20a <sub>1</sub>		10	2.0/good, uniform cell structure.	--	--	--	--	2.0	1.40	0.195	
20a <sub>2</sub>	Gaco Neoprene-Hypalon over unknown existing coating/CPR 425 foam	10	2.0/good, uniform cell structure	--	--	--	--	1.75	1.25	0.192	Foam may have been uncoated for some time before Neo- prene-Hypalon applied.
Samples from NCEL, Port Hueneme, California											
21a <sub>1</sub>	Irrthane 300/394 Ure- thane/CPR Upjohn 485-2.0	4-3/4	2.0/good, uniform cell structure.	10 (P)	--	--	20 (P)	2.25	1.58	0.130	Coating is chalking to point where base coat starting to show. Coating flexible and in condition otherwise.
21a <sub>2</sub>		4-3/4	2.0/good, uniform cell structure	10 (P)	--	--	20 (P)	2.25	1.58	0.140	0.135
21b	Irrthane 300/394 Ure- thane/CPR Upjohn 485-3.0	4-3/4	3.0/good, uniform cell structure	6 (P)	6 (P)	--	12 (P)	2.50	1.76	0.134	Same as Sample 21a <sub>2</sub>
21c	Irrthane 300/157 Ure- thane/Hypalon CPR Upjohn 485-2.0	4-3/4	2.0/good, uniform cell structure	5 (P)	4 (I)	--	9 (I)	2.00	1.17	0.144	Topcoat chalking heavily with pin holes to base coat. Coating flexible in good condition.
21d	Irrthane 300/157 Ure- thane/Hypalon CPR Upjohn 485-3.0	4-3/4	3.0/good, uniform cell structure	8 (P)	6 (I)	--	14 (I)	2.25	1.35	0.144	Very rough foam surface. Coating same as Sample 22a.

continued

Table 1. *Continued*

Sample No.	Roof Coating/Foam System	Age (yr)	Foam Density (pcf) and Quality	Coating Thickness (mils) <sup>b</sup>			Foam Thickness (in.) <sup>b</sup>	Comments		
				First Coat	Second Coat	Third Coat	Total	Roof (Avg)	Individual Sample	Average
22a <sub>1</sub>	Monolac Mastic Hypalon/CPR Upjohn 485-2.5	7	2.5/good, uniform cell structure.	14 (1)	--	--	14 (1)	2.00	1.33	0.140
22a <sub>2</sub>	Monolac Mastic Hypalon/CPR Upjohn 485-2.5	7	2.5/good, uniform cell structure	14 (1)	--	--	14 (1)	2.00	1.27	0.145
22b	Monolac Mastic Hypalon/CPR Upjohn 485-2.5	7	2.5/good, uniform cell structure.	11 (1)	--	--	11 (1)	2.00	1.22	0.148
23a <sub>1</sub>	Diatom Acrylic/CPR Upjohn 485-2.5	7-1/4	2.5/good, uniform cell structure	25 (P)	--	--	25 (P)	1.25	0.79	0.180
23a <sub>2</sub>	Diatom Acrylic/CPR Upjohn 485-2.5	7-1/4	2.5/good, uniform cell structure	25 (P)	--	--	25 (P)	1.25	0.58	0.196
23b <sub>1</sub>	Diatom Acrylic/CPR Upjohn 485-2.5	7-1/4	2.5/good, uniform cell structure	20 (P)	--	--	20 (P)	1.75	1.04	0.199
23b <sub>2</sub>	Diatom Acrylic/CPR Upjohn 485-2.5	7-1/4	2.5/good, uniform cell structure	20 (P)	--	--	20 (P)	1.75	0.81	0.167
24a <sub>1</sub>	United Coatings Butyl-Hypalon/CPR Upjohn 485-2.5	7-1/6	2.5/good, uniform cell structure	29 (1)	15 (1)	--	44 (1)	1.50	1.02	0.181
24a <sub>2</sub>	United Coatings Butyl-Hypalon/CPR Upjohn 485-2.5	7-1/6	2.5/good, uniform cell structure	29 (1)	15 (1)	--	44 (1)	1.50	0.93	0.184
24b	United Coatings Butyl-Hypalon/CPR Upjohn 485-2.5	7-1/6	2.5/good, uniform cell structure	15 (1)	9 (1)	--	24 (1)	2.25	1.66	0.165
25a	General Electric Silicone with Granules/CPR Upjohn 485-2.5	7	2.5/good, uniform cell structure	7.5 (P)	7.5 (P)	--	15.0 (P)	1.75	1.48	0.164
25b	General Electric Silicone with Granules/CPR Upjohn 485-2.5	7	2.5/good, uniform cell structure	11 (P)	11 (P)	--	22 (P)	1.75	1.39	0.146

continued

Table 1. Continued

Sample No.	Roof Coating/Foam System Description	Age (yr)	Foam Density (pcf) and Quality	Coating Thickness (mils) <sup>b</sup>			Foam Thickness (in.)	Thermal Conductivity (Btu/hr-ft <sup>2</sup> -°F/in.)	Comments		
				First Coat	Second Coat	Third Coat	Roof (Avg)	Individual Sample			
25c	General Electric Silicone w/o Granules/CPR Upjohn 485-2.5	7	2.5/good, uniform cell structure	9.5 (P)	9.5 (P)	-- (P)	19.0 (P)	2.00	1.65	0.157	Same as Sample 26a except that dirt is more obvious.
25d	General Electric Silicone w/o Granules/CPR Upjohn 485-2.5	7	2.5/good, uniform cell structure	7.5 (P)	7.5 (P)	-- (P)	15.0 (P)	2.00	1.53	0.140	Same as Sample 26a.
26a	Gaco N-118 Neoprene + H-10 Hypalon/CPR Upjohn 485-2.5	7	2.5/good, uniform cell structure	8 (I)	8 (I)	-- (I)	16 (I)	1.50	1.37	0.137	Heavy chalking of top coat; base coat showing through. Overall coating is flexible and in good condition.
26b <sub>1</sub>	Gaco N-118 Neoprene + H-10 Hypalon/CPR Upjohn 485-2.5	7	2.5/good, uniform cell structure	10 (I)	8 (I)	-- (I)	18 (I)	1.50	0.90	0.162	Same as Sample 26a, except that topcoat is cratered.
26b <sub>2</sub>		7	2.5/good, uniform cell structure	10 (I)	8 (I)	-- (I)	18 (I)	1.50	0.56	0.172	
27a	Rapid Roof with Granules/ CPR Upjohn 480-2.5	1-1/4	2.5/good, uniform cell structure	25 (P)	30 (P)	-- (P)	55 (P)	2.25	2.08	0.111	Coating in good condition.
27b	Rapid Roof with Granules/ CPR Upjohn 480-2.5	1-1/4	2.5/good, uniform cell structure	28 (P)	29 (P)	-- (P)	57 (P)	2.00	1.74	0.129	Coating in good condition.
28a	Rooflex 155/CPR Upjohn 485-2.5	4-5/6	2.5/good, uniform cell structure. Foam surface sunburnt	36 (P)	-- (P)	-- (P)	36 (P)	2.00	1.89	0.155	Coating cratered, flexible, and in good condition. Foam surface sunburnt.
28b	Rooflex 155/CPR Upjohn 485-2.5	4-5/6	2.5/good, uniform cell structure	30 (P)	-- (P)	-- (P)	30 (P)	2.00	1.88	0.136	Coating cratered, breaks easily. Some areas worn through to foam; fair condition.

continued

Table 1. Continued

Sample No.	Roof Coating/Foam System Description	Age (yr)	Foam Density (pcf) and Quality	Coating Thickness (mils) <sup>b</sup>			Foam Thickness (in.)	Thermal Conductivity (Btu/hr-ft <sup>2</sup> -°F/in.)	Comments		
				First Coat	Second Coat	Third Coat					
29 <sub>a</sub> <sub>1</sub>	Foam Systems Arylicflex/ FSC-26-3.0	1-1/4	3.0/good, uniform cell structure	16 (P)	10 (P)	--	26 (P)	1.50	0.82	0.157	Coating, although maintaining some flexibility, is almost brittle; breaks easily; fair condition.
29 <sub>a</sub> <sub>2</sub>		1-1/4	3.0/good, uniform cell structure	16 (P)	10 (P)	--	26 (P)	1.50	0.70	0.162	

<sup>a</sup>The number refers to a building (roof) or panel where a sample was taken, the letter following the number refers to sample taken from a different area. Numbers (if any) refer to the specimens cut out of the sample when more than one specimen was cut and tested from a given sample.

<sup>b</sup>P = permeable; I = impermeable.

<sup>c</sup>Sample numbers for Samples 1 through 5 are the same as those given systems in Reference 1.

Table 2. Average k-Values and Ages of PUF Samples

Area	PUF with Permeable Coatings			PUF with Impermeable Coatings			Overall Averages		
	Average k-Value (Btu/hr-ft <sup>2</sup> -°F/in.)	Average Age (yr.)	Number of Samples	Average k-Value (Btu/hr-ft <sup>2</sup> -°F/in.)	Average Age (yr.)	Number of Samples	k-Value (Btu/hr-ft <sup>2</sup> -°F/in.)	Age (yr.)	Number of Samples
Chicago	0.170 ± 0.030	5.0	8	0.146 ± 0.008	5.0	8	0.158 ± 0.015	5.0	16
Denver	0.191 ± 0.012	7.1 ± 2.4	5	0.180 ± 0.016	10.1 ± 0.5	2	0.188 ± 0.013	8.0 ± 2.8	7
San Francisco Bay	0.175 ± 0.011	5.2 ± 1.0	6	---	---	---	0.175 ± 0.013	5.2 ± 1.09	6
Guam	0.193	7	1	---	---	---	0.191 ± 0.005	8.3 ± 2.9	3 <sup>a</sup>
NCEL	0.153 ± 0.024	5.0 ± 2.4	11	0.156 ± 0.017	6.6 ± 0.9	11	0.154 ± 0.021	5.7 ± 2.1	28
Total	0.164 ± 0.023	5.8 ± 3.4	17	0.158 ± 0.017	7.1 ± 3.0	21	0.163 ± 0.022	5.8 ± 2.1	60 <sup>a</sup>

<sup>a</sup>Total averages include two samples of an unknown type of coating from Guam but do not include Sample 19, also from Guam.

Table 3. Thermal Conductivity k-Values of NCEL Samples in Increasing Order

Sample Number	Coating Thickness (mils) <sup>a</sup>	Coating <sup>b</sup>	Foam Density (pcf)	Foam Thickness (in.)		Thermal Conductivity		Roof age (yrs)
				Roof (avg)	Sample	Individual	Average	
27a	25/30:55	P	2.5	2.25	2.08	0.111		1-1/4
27b	28/29:57	P	2.5	2.00	1.74	0.129		1-1/4
21b	6/6:12	P	2.0	2.50	1.76	0.134		4-3/4
21a <sub>1</sub> 21a <sub>2</sub>	10/10:20	P	2.0	2.25	1.58	0.130	0.135	4-3/4
28b	30:30	P	2.5	2.00	1.88	0.136		4-5/6
26a	8/8:16	I	2.5	1.50	1.37	0.137		7
25d	7.5/7.5:15	P	2.5	2.00	1.53	0.140		7
22a <sub>1</sub> 22a <sub>2</sub>	14:14	I	2.5	2.00	1.33	0.140	0.1425	7
21d	8/6:14	P/I	2.0	2.25	1.35	0.144		4-3/4
21c	5/4:9	P/I	2.0	2.00	1.17	0.144		4-3/4
25b	11/11:22	P	2.5	1.75	1.39	0.146		7
22b	11:11	I	2.5	2.00	1.22	0.148		7
28a	36:36	P	2.5	2.00	1.89	0.155		4-5/6
25c	9.5/9.5:19	P	2.5	2.00	1.65	0.157		7
29a <sub>1</sub> 29a <sub>2</sub>	16/10:26	P	3.0	1.50 1.50	0.82 0.70	0.157 0.162	0.1595	1-1/4
25a	7.5/7.5:15	P	2.5	1.75	1.48	0.164		~
24b	15/9:24	I	2.5	2.25	1.66	0.165		1-1/4
26b <sub>1</sub> 26b <sub>2</sub>	10/8:18	I	2.5	1.50 1.50	0.90 0.56	0.162 0.172	0.167	
24a <sub>1</sub> 24a <sub>2</sub>	29/15:44	I	2.5	1.50 1.50	1.02 0.93	0.181 0.184	0.181	~
23b <sub>1</sub> 23b <sub>2</sub>	20:20	P	2.5	1.75 1.75	1.04 0.81	0.199 0.167	0.183	1-1/4
23a <sub>1</sub> 23a <sub>2</sub>	25:25	P	2.5	1.25 1.25	0.79 0.58	0.180 0.196	0.188	1-1/4

<sup>a</sup> First coat/second coat:total

<sup>b</sup> P = permeable; I = impermeable

Table 4. k-Values for a 2.2 pcf PUF

Age of Samples (yr)	Predicted <sup>a</sup> k-Value for Following Foam Thicknesses	
	1 in.	2 in.
5	0.158	0.148
7	0.165	0.150
10	0.175	0.154

<sup>a</sup>From Reference 6. Samples are 12 x 12 x 1 or 2 inches, aged at 25°C (77°F), under controlled atmospheric conditions with all sides exposed.

Table 5. Actual Average k-Values for NCEL Field-Aged PUF Samples

Coating Type	5-Year Old Sample		7-Year Old Samples	
	PUF Thickness (in.)	Average k-Value	PUF Thickness (in.)	Average k-Value
Permeable	2.20 ± 0.21	0.139 ± 0.010	1.69 ± 0.29	0.169 ± 0.022
	2.0 only	0.145 ± 0.013	2.0 only	0.148 ± 0.012
Impermeable	2.12 ± 0.18	0.144	1.75 ± 0.31	0.159 ± 0.018
	2.0 only	0.144	2.0 only	0.144 ± 0.004
Overall	2.18 ± 0.010	0.140 ± 0.008	1.72 ± 0.29	0.164 ± 0.020
	2.0 only	0.145 ± 0.010	2.0 only	0.146 ± 0.007

Table 6. k-Values of all Samples in Increasing Order

Area <sup>a</sup>	Sample Number	Coating Thickness (mil)	Coating <sup>c</sup>	Foam Density (pcf)	Foam Thickness (in.)			Thermal Conductivity		Roof (age) (yr)
					Roof (avg)	k-Sample	Individual	Average		
N	27a	25/30/-:55	P	2.5	2.25	2.08	0.111			1-1/4
N	27b	28/29/-:57	P	2.5	2.00	1.74	0.129			1-1/4
N	21b	6/6/-:12	P	2.0	2.50	1.76	0.134			4-3/4
N	21a <sub>1</sub>	10/10/-:20	P	2.0	2.25	1.58	0.130			4-3/4
N	21a <sub>2</sub>	10/10/-:20	P	2.0	2.25	1.58	0.140			4-3/4
N	28b	30/-/-:30	P	2.5	2.00	1.88	0.136			4-5/6
N	26a	8/8:16	I	2.5	1.50	1.37	0.137			7
C	4b <sub>1</sub>	20/10/15:45	I/P/P	2.0	2.25	1.50	0.143			5
C	4b <sub>2</sub>	20/10/15:45	I/P/P	2.0	2.25	1.48	0.135			5
N	25d	7.5/7.5:15	P	2.5	2.00	1.53	0.140			7
C	5a <sub>1</sub>	5/10/-:15	I/P	2.0	2.25	1.51	0.144			5
C	5a <sub>2</sub>	5/10/-:15	I/P	2.0	2.25	1.48	0.137			5
N	22a <sub>1</sub>	14/-/-:14	I	2.5	2.00	1.33	0.140			7
N	22a <sub>2</sub>	14/-/-:14	I	2.5	2.00	1.27	0.145			7
N	21d	8/6/-:14	P/I	2.0	2.25	1.35	0.144			4-3/4
N	21c	5/4/-:9	P/I	2.0	2.00	1.17	0.144			4-3/4
N	25b	11/11/-:22	P	2.5	1.75	1.39	0.146			7
C	4a <sub>1</sub>	15/20/20:55	I/P/P	2.0	2.00	1.37	0.148			5
C	4a <sub>2</sub>	15/20/20:55	I/P/P	2.0	2.00	1.37	0.146			5
N	22b	11/-/-:11	I	2.5	2.00	1.22	0.148			7
N	28a	36/-/-:36	P	2.5	2.00	1.89	0.155			4-5/6
C	1b <sub>1</sub>	15/5/-:55	P	2.0	2.00	1.37	0.156			5
C	1b <sub>2</sub>	15/5/-:55	P	2.0	2.00	1.35	0.156			5
N	25c	9.5/9.5/-:19	P	2.5	2.00	1.65	0.157			7
C	3a <sub>1</sub>	10/5/-:15	I/P	2.0	2.25	1.42	0.160			5
C	3a <sub>2</sub>	10/5/-:15	I/P	2.0	2.25	1.58	0.155			5
N	29a <sub>1</sub>	16/10/-:26	P	3.0	1.50	0.82	0.157			1-1/4
N	29a <sub>2</sub>	16/10/-:26	P	3.0	1.50	0.70	0.162			1-1/4

continued

Table 6. Continued

Area <sup>a</sup>	Sample Number	Coating Thickness (mil) <sup>b</sup>	Coating C	Foam Density (pcf)	Foam Thickness (in.)	Thermal Conductivity		Roof (age) (yr)
						Roof (avg)	k-Sample	
C	16a <sub>1</sub>	10/-/-:26	P	2.0	2.00	1.37	0.168	4
C	16a <sub>2</sub>	10/-/-:26	P	2.0	2.00	1.62	0.154	4
N	25a	7.5/7.5/-:15	P	2.5	1.75	1.48	0.164	7
N	24b	15/9/-:24	1	2.5	2.25	1.66	0.165	7-1/6
N	26b <sub>1</sub>	10/8/-:18	1	2.5	1.50	0.90	0.162	7
N	26b <sub>2</sub>	10/8/-:18	1	2.5	1.50	0.56	0.172	7
D	9	2/5/-:7	I	2.0	1.50	1.15	0.169	9-3/4
D	8	15/-/-:7	P	2.0	2.00	1.57	0.170	9-3/4
C	2a <sub>1</sub>	7/-/-:7	P	2.0	1.75	1.09	0.175	5
C	2a <sub>2</sub>	7/-/-:7	P	2.0	1.75	1.09	0.169	5
S	17	15/-/-:15	P	2.0	1.50	1.06	0.173	5
C	2b <sub>1</sub>	10/10/-:20	P	2.0	2.25	1.57	0.180	5
C	2b <sub>2</sub>	10/10/-:20	P	2.0	2.25	1.58	0.171	0.1755
C	1a <sub>1</sub>	10/10/-:20	P	2.0	2.00	1.32	0.181	5
C	1a <sub>2</sub>	10/10/-:20	P	2.0	2.00	1.46	0.175	5
S	14	15/-/-:15	P	(?)	1.25	0.65	0.182	6
N	24a <sub>1</sub>	29/15/-:44	J	2.5	1.50	1.02	0.181	0.1825
N	24a <sub>2</sub>	29/15/-:44	I	2.5	1.50	0.93	0.184	7-1/6
N	23b <sub>1</sub>	20/-/-:20	P	2.5	1.75	1.04	0.199	7-1/4
N	23b <sub>2</sub>	20/-/-:20	P	2.5	1.75	0.81	0.167	7-1/4
S	13	15/-/-:15	P	(?)	1.25	0.77	0.186	6
N	23a <sub>1</sub>	25/-/-:25	P	2.5	1.25	0.79	0.180	7-1/4
N	23a <sub>2</sub>	25/-/-:25	P	2.5	1.25	0.58	0.196	7-1/4
G	20a <sub>1</sub>	-/-/-:-	P	2.0	2.00	1.40	0.185	10
G	20a <sub>2</sub>	-/-/-:-	P	2.0	1.75	1.25	0.192	10
S	15	-/-/-:-	P	(?)	1.75	1.26	0.189	6
D	10	10/10/-:20	P	2.0	2.00	1.54	0.189	4-1/3

continued

Table 6. Continued

Area <sup>a</sup>	Sample Number	Coating Thickness (mil)	Coating <sup>c</sup>	Foam Density (pcf)	Foam Thickness (in.)	Thermal Conductivity		Roof (age) (yr)
						Roof (avg)	k-Sample	
C	16a <sub>1</sub>	10/-/-:26	P	2.0	2.00	1.37	0.168	4
C	16a <sub>2</sub>	10/-/-:26	P	2.0	2.00	1.62	0.154	4
N	25a	7.5/7.5/-:15	P	2.5	1.75	1.48	0.164	7
N	24b	15/9/-:24	I	2.5	2.25	1.66	0.165	7-1/6
N	26b <sub>1</sub>	10/8/-:18	I	2.5	1.50	0.90	0.162	7
N	26b <sub>2</sub>	10/8/-:18	I	2.5	1.50	0.56	0.172	0.167
D	9	2/5/-:7	I	2.0	1.50	1.15	0.169	9-3/4
D	8	15/-/-:7	P	2.0	2.00	1.57	0.170	9-3/4
C	2a <sub>1</sub>	7/-/-:7	P	2.0	1.75	1.09	0.175	5
C	2a <sub>2</sub>	7/-/-:7	P	2.0	1.75	1.09	0.169	0.172
S	17	15/-/-:15	P	2.0	1.50	1.06	0.173	5
C	2b <sub>1</sub>	10/10/-:20	P	2.0	2.25	1.57	0.180	5
C	2b <sub>2</sub>	10/10/-:20	P	2.0	2.25	1.58	0.171	0.1755
C	1a <sub>1</sub>	10/10/-:20	P	2.0	2.00	1.32	0.181	5
C	1a <sub>2</sub>	10/10/-:20	P	2.0	2.00	1.46	0.175	5
S	14	15/-/-:15	P	(?)	1.25	0.65	0.182	6
N	24a <sub>1</sub>	29/15:44	I	2.5	1.50	1.02	0.181	7-1/6
N	24a <sub>2</sub>	29/15:44	I	2.5	1.50	0.93	0.184	0.1825
N	23b <sub>1</sub>	20/-/-:20	P	2.5	1.75	1.04	0.199	7-1/6
N	23b <sub>2</sub>	20/-/-:20	P	2.5	1.75	0.81	0.167	0.183
S	13	15/-/-:15	P	(?)	1.25	0.77	0.186	6
N	23a <sub>1</sub>	25/-/-:25	P	2.5	1.25	0.79	0.180	7-1/4
N	23a <sub>2</sub>	25/-/-:25	P	2.5	1.25	0.58	0.196	0.188
G	20a <sub>1</sub>	-/-/-:-	P	2.0	2.00	1.40	0.185	10
G	20a <sub>2</sub>	-/-/-:-	P	2.0	1.75	1.25	0.192	0.1885
S	15	-/-/-:-	P	(?)	1.75	1.26	0.189	6
D	10	10/10/-:20	P	2.0	2.00	1.54	0.189	4-1/3

continued

Table 6. Continued

Area <sup>a</sup>	Sample Number	Coating Thickness (mil)	Coating <sup>c</sup>	Foam Density (pcf)	Foam Thickness (in.)	Thermal Conductivity		Roof (age) (yr)
						Roof (avg)	Sample k-	
D	7	3/-/-3	I	2.0	1.50	1.08	0.191	10-1/2
D	12	10/10/-20	P	2.0	2.00	1.67	0.194	6-1/2
G	18	5/-/-5	P	2.0	1.25	0.66	0.195	5
D	11	150/20/5:175	P	2.0	2.00	1.56	0.198	4-1/3
D	6	12/-/-12	P	2.0	1.50	1.12	0.202	10-1/2
G	19	12/-/-12	P	2.0/3.0	1.00	0.56	0.259	4-1/3

<sup>a</sup>H = NCEI, Port Hueneme; C = Clifton, S = Subic Bay; D = Denver; G = Guam<sup>b</sup>First coat/second coat/third coat: total - Dashes indicate further coatings were not used<sup>c</sup>P = permeable; I = impermeable

## DISTRIBUTION LIST

ARMY Fal Engr, Letterkenny Army Depot, Chambersburg, PA  
AFB (AFIT/LDE), Wright Patterson OH; (RDVA) AFESC/R&D Tyndall, FL; 82ABG/DEMC, Williams AZ;  
ABG/DEE (F. Nethers), Goodfellow AFB TX; AF Tech Office (Mgt & Ops), Tyndall, FL; CESCH,  
Wright-Patterson; HQ Tactical Air Cmd/DEMM (Schmidt) Langley, VA; LEEH (J Stanton) Washington,  
DC; MAC/DET, Scott, IL; SAMSO/MNND, Norton AFB CA; Samso/Dec (Sauer) Vandenburg, CA; Stinfo  
Library, Offutt NE  
AFESC DEB, Tyndall, FL  
ARMY ARRADCOM, Dover, NJ; BMDSC-RE (H. McClellan) Huntsville AL; Contracts - Facs Engr  
Directorate, Fort Ord, CA; DAEN-CWE-M, Washington DC; DAEN-MPE-D Washington DC;  
DAEN-MPO-U, Washington, DC; DAEN-MPU, Washington DC; ERADCOM Tech Supp Dir. (DELSD-L)  
Ft. Monmouth, NJ; Natick R&D Command (Kwoh Hu) Natick MA; Tech. Ref. Div., Fort Huachuca, AZ  
ARMY - CERL Library, Champaign IL  
ARMY COASTAL ENGR RSCH CEN Fort Belvoir VA; R. Jachowski, Fort Belvoir VA  
ARMY COE Philadelphia Dist. (LIBRARY) Philadelphia, PA  
ARMY CORPS OF ENGINEERS Fac Engr Supp Agency, Ft. Belvoir, VA; MRD-Eng. Div., Omaha NE;  
Seattle Dist. Library, Seattle WA  
ARMY CRREL Constr. Engr Res Branch, (Aamot); G. Phetteplace Hanover, NH  
ARMY CRREL R.A. Eaton  
ARMY ENG DIV HNDED-CS, Huntsville AL; HNDED-FD, Huntsville, AL  
ARMY ENG WATERWAYS EXP STA Library, Vicksburg MS  
ARMY ENGR DIST. Library, Portland OR  
ARMY ENVIRON. HYGIENE AGCY HSE-EW Water Qual Eng Div Aberdeen Prov Grnd MD  
ARMY MATERIALS & MECHANICS RESEARCH CENTER Dr. Lenoe, Watertown MA  
ARMY MISSILE R&D CMD SCI Info Cen (DOC) Redstone Arsenal, AL  
ARMY MTMC Trans Engr Agency MTT-CE, Newport News, VA  
ARMY-DEPOT SYS COMMAND DRSDS-AI Chambersburg, PA  
ASO PWD (ENS M W Davis), Philadelphia, PA  
BUREAU OF RECLAMATION Code 1512 (C. Selander) Denver CO  
CINCLANT CIV ENGR SUPP PLANS OFFR NORFOLK, VA  
CINCPAC Fac Engrng Div (J44) Makalapa, HI  
CNAVRES Code 13 (Dir. Facilities) New Orleans, LA  
CNM Code MAT-04, Washington, DC; Code MAT-Q8E, Washington, DC; NMAT - 044, Washington DC  
CNO Code NOP-964, Washington DC; Code OP 987 Washington DC; Code OP-413 Wash, DC; Code OPNAV  
09B24 (H); OP-098, Washington, DC; OP987J, Washington, DC  
COMCBPAC Operations Off, Makalapa HI  
COMFLEACT, OKINAWA PWD - Engr Div, Sasebo, Japan; PWO, Kadena, Okinawa; PWO, Sasebo, Japan  
COMNAVAIRLANT NUC Wpns Sec Offr Norfolk, VA  
COMNAVAMARIANAS Code N4, Guam  
COMOCEANSYSLANT PW-FAC MGMT Off Norfolk, VA  
COMOCEANSYSPAC SCE, Pearl Harbor HI  
COMSUBDEVGRUONE Operations Offr, San Diego, CA  
DEFFUELUPPCEN DFSC-OWE (Term Engrng) Alexandria, VA; DFSC-OWE, Alexandria VA  
DOE F.F. Parry, Washington DC; INEL Tech. Lib. (Reports Section), Idaho Falls, ID  
DTIC Defense Technical Info Ctr/Alexandria, VA  
DTNSRDC Anna Lab, Code 4121 (R A Rivers) Annapolis, MD  
DTNSRDC Code 172 (M. Krenzke), Bethesda MD  
DTNSRDC Code 284 (A. Rufolo), Annapolis MD  
DTNSRDC Code 4111 (R. Gierich), Bethesda MD; Code 42, Bethesda MD  
DTNSRDC Code 522 (Library), Annapolis MD  
ENVIRONMENTAL PROTECTION AGENCY Reg. III Library, Philadelphia PA; Reg. VIII, 8M-ASL,  
Denver CO  
FLTCOMBATTRACENLANT PWO, Virginia Bch VA  
FMFLANT CEC Offr, Norfolk VA  
GSA Assist Comm Des & Cnst (FAIA) D R Dibner Washington, DC ; Off of Des & Const-PCDP (D Eakin)  
Washington, DC  
HC & RS Tech Pres. Service, Meden, Washington, DC  
KWAJALEIN MISRAN BMDSC-RKL-C  
LIBRARY OF CONGRESS Washington, DC (Sciences & Tech Div)  
MARINE CORPS BASE Code 406, Camp Lejeune, NC; M & R Division, Camp Lejeune NC; Maint Off Camp  
Pendleton, CA; PWD - Maint. Control Div. Camp Butler, Kawasaki, Japan; PWO Camp Lejeune NC;  
PWO, Camp Pendleton CA; PWO, Camp S. D. Butler, Kawasaki Japan  
MARINE CORPS HQS Code LFF-2, Washington DC

MCAS Facil. Engr. Div. Cherry Point NC; CO, Kaneohe Bay HI; Code S4, Quantico VA; Facs Maint Dept - Operations Div. Cherry Point; PWD - Utilities Div, Iwakuni, Japan; PWD, Dir. Maint. Control Div., Iwakuni Japan; PWO, Iwakuni, Japan; PWO, Yuma AZ

MCDEC M&L Div Quantico VA; NSAP REP, Quantico VA

MCLB B520, Barstow CA; Maintenance Officer, Barstow, CA; PWO, Barstow CA

MCRD PWO, San Diego Ca

NAF PWD - Engr Div, Atsugi, Japan; PWO, Atsugi Japan

NALF OINC, San Diego, CA

NARF Code 100, Cherry Point, NC; Code 612, Jax, FL; Code 640, Pensacola FL; Equipment Engineering Division (Code 61000), Pensacola, FL

NAS CO, Guantanamo Bay Cuba; Code 114, Alameda CA; Code 183 (Fac. Plan BR MGR); Code 18700, Brunswick ME; Code 18U (ENS P.J. Hickey), Corpus Christi TX; Code 6234 (G. Trask), Point Mugu CA; Code 70, Atlanta, Marietta GA; Code 8E, Patuxent Riv., MD; Dir of Engrng, PWD, Corpus Christi, TX; Dir. Maint. Control Div., Key West FL; Dir. Util. Div., Bermuda; Grover, PWD, Patuxent River, MD; Lakehurst, NJ; Lead. Chief. Petty Offr. PW/Self Help Div, Beaville TX; OIC, CBU 417, Oak Harbor WA; PW (J. Maguire), Corpus Christi TX; PWD - Engr Div Dir, Millington, TN; PWD - Engr Div, Gtmo, Cuba; PWD - Engr Div, Oak Harbor, WA; PWD Maint. Cont. Dir., Fallon NV; PWD Maint. Div., New Orleans, Belle Chasse LA; PWD, Code 1821H (Pfankuch) Miramar, SD CA; PWD, Maintenance Control Dir., Bermuda; PWD, Willow Grove PA; PWO Belle Chasse, LA; PWO Chase Field Beaville, TX; PWO Key West FL; PWO Lakehurst, NJ; PWO Sigonella Sicily; PWO Whiting Fld, Milton FL; PWO, Cubi Point, R.P.; PWO, Dallas TX; PWO, Glenview IL; PWO, Kingsville TX; PWO, Millington TN; PWO, Miramar, San Diego CA; PWO, Moffett Field CA

NAVFACENGC COM CONTRACTS ROICC Key West FL

NAS SCE Norfolk, VA; SCE Norfolk, VA; SCE, Barbers Point HI; Security Offr, Alameda CA

NASDC-WDC T. Fry, Manassas VA

NATL BUREAU OF STANDARDS B-348 BR (Dr. Campbell), Washington DC

NATL RESEARCH COUNCIL Naval Studies Board, Washington DC

NAVACT PWO, London UK

NAVACTDET PWO, Holy Lock UK

NAVAEROSPREGMEDCEN SCE, Pensacola FL

NAVAIRDEVcen Chmielewski, Warminster, PA; Code 813, Warminster PA; PWD, Engr Div Mgr, Warminster, PA

NAVAIRPROPTESTCEN CO, Trenton, NJ

NAVAVIONICFAC PW Div Indianapolis, IN; PWD Deputy Dir. D/701, Indianapolis, IN

NAVAVNWPNSFAC Wpns Offr, St. Mawgan, England

NAVCAPGRU Engineering Officer, Code 60 Williamsburg, VA

NAVCOASTSYCEN CO, Panama City FL; Code 423 Panama City, FL; Code 715 (J Quirk) Panama City, FL; Code 715 (J. Mittleman) Panama City, FL; Library Panama City, FL; PWO Panama City, FL

NAVCOMMAREAMSTRSTA Code W-60, Elec Engr, Wahiawa, HI; PWO, Norfolk VA; SCE Unit 1 Naples Italy; SCE, Wahiawa HI

NAVCOMMSTA Code 401 Nea Makri, Greece; PWD - Maint Control Div, Diego Garcia Is.; PWO, Exmouth, Australia; SCE Balkoa, Panama Canal

NAVCONSTRACEN Curriculum/Instr. Stds Offr, Gulfport MS

NAVEDTRAPRODEVcen Technical Library, Pensacola, FL

NAVEDUTRACEN Engr Dept (Code 42) Newport, RI

NAVENVIRHLTHCEN CO, NAVSTA Norfolk, VA

NAVEODTECHCEN Code 605, Indian Head MD

NAVFAC PWO, Brawdy Wales UK; PWO, Centerville Bch, Ferndale CA; PWO, Point Sur, Big Sur CA; SCE NAVFACENGC COM Code 03T (Essoglou) Alexandria, VA; Code 043 Alexandria, VA; Code 044 Alexandria, VA; Code 0453 (D. Potter) Alexandria, VA; Code 046; Code 0461D (V M Spaulding) Alexandria, VA; Code 04A1 Alexandria, VA; Code 04B3 Alexandria, VA; Code 051A Alexandria, VA; Code 09M54, Technical Library, Alexandria, VA; Code 100 Alexandria, VA; Code 1002B (J. Leimanis) Alexandria, VA; Code 1113, Alexandria, VA; Code 111A Alexandria, VA

NAVFACENGC COM CONTRACTS ROICC, Yap; ROICC Code 495 Portsmouth VA

NAVFACENGC COM code 08T Alexandria, VA

NAVFACENGC COM - CHES DIV. Code 101 Wash, DC; Code 403 Washington DC; Code 405 Wash, DC; Code 407 (D Scheesele) Washington, DC; Code FPO-1C Washington DC; Contracts, ROICC, Annapolis MD; FPO-1 Washington, DC; FPO-1EAS Washington DC; Library, Washington, D.C.

NAVFACENGC COM - LANT DIV. Code 111, Norfolk, VA; Code 403, Norfolk, VA; Eur. BR Deputy Dir, Naples Italy; Library, Norfolk, VA; RDT&ELO 102A, Norfolk, VA

NAVFACENGC COM - NORTH DIV. CO; Code 04 Philadelphia, PA; Code 09P Philadelphia PA; Code 1028, RDT&ELO, Philadelphia PA; Code 111 Philadelphia, PA; Code 4012/AB (A. Bianchi) Philadelphia, PA; Library, Philadelphia, PA; ROICC, Contracts, Crane IN

NAVFACENGC COM - PAC DIV. (Kyi) Code 101, Pearl Harbor, HI; CODE 09P PEARL HARBOR HI; Code 2011 Pearl Harbor, HI; Code 402, RDT&E, Pearl Harbor HI; Commander, Pearl Harbor, HI; Library, Pearl Harbor, HI

NAVFACENGCOM - SOUTH DIV. Code 403, Gaddy, Charleston, SC; Code 405 Charleston, SC; Code 411  
Soil Mech & Paving BR Charleston, SC; Code 90, RDT&ELO, Charleston SC; Library, Charleston, SC  
NAVFACENGCOM - WEST DIV. 102; AROICC, Contracts, Twentynine Palms CA; Code 04B San Bruno, CA  
NAVFACENGCOM CONTRACTS Contracts, AROICC, Lemoore CA  
NAVFACENGCOM - WEST DIV. Library, San Bruno, CA; O9P/20 San Bruno, CA; RDT&ELO Code 2011  
San Bruno, CA  
NAVFACENGCOM CONTRACTS AROICC MCAS El Toro; AROICC, NAVSTA Brooklyn, NY; AROICC,  
Point Mugu CA; AROICC, Quantico, VA; Colts Neck, NJ; Dir, Eng. Div., Exmouth, Australia; Eng Div  
dir, Southwest Pac, Manila, PI; NAS, Jacksonville, FL; OICC, Southwest Pac, Manila, PI; OICC-ROICC,  
NAS Oceana, Virginia Beach, VA; OICC/ROICC, Balboa Panama Canal; ROICC AF Guam; ROICC,  
Diego Garcia Island; ROICC, Keflavik, Iceland; ROICC, NAS, Corpus Christi, TX; ROICC, Pacific, San  
Bruno CA; ROICC-OICC-SPA, Norfolk, VA  
NAVHOSP PWD - Engr Div, Beaufort, SC  
NAVMAG PWD - Engr Div, Guam; SCE, Guam; Subic Bay, R.P.  
NAVOCEANO Code 3432 (J. DePalma), Bay St. Louis MS; Library Bay St. Louis, MS  
NAVOCEANSYSCEN Code 4473 Bayside Library, San Diego, CA; Code 4473B (Tech Lib) San Diego, CA;  
Code 5221 (R.Jones) San Diego Ca; Code 523 (Hurley), San Diego, CA; Code 6700, San Diego, CA; Code  
811 San Diego, CA  
NAVORDMISTESTFAC PWD - Engr Dir, White Sands, NM  
NAVORDSTA PWD - Dir, Engr Div, Indian Head, MD; PWO, Louisville KY  
NAVPETOFF Code 30, Alexandria VA  
NAVPETRES Director, Washington DC  
NAVPHIBASE CO, ACB 2 Norfolk, VA; Code S3T, Norfolk VA; Harbor Clearance Unit Two, Little Creek,  
VA  
NAVFACENGCOM CONTRACTS OICC/ROICC, Norfolk, VA  
NAVPHIBASE SCE Coronado, SD, CA  
NAVRADRECFAC PWO, Kami Seya Japan  
NAVREGMEDCEN Code 3041, Memphis, Millington TN; PWD - Engr Div, Camp Lejeune, NC; PWO, Camp  
Lejeune, NC; SCE Newport RI; PWO Portsmouth, VA  
NAVREGMEDCEN PWO, Okinawa, Japan  
NAVREGMEDCEN SCE; SCE San Diego, CA; SCE, Camp Pendleton CA; SCE, Guam; SCE, Oakland CA  
NAVREGMEDCEN SCE, Yokosuka, Japan  
NAVSOLCECOFF C35 Port Hueneme, CA; CO, Code C44A Port Hueneme, CA  
NAVSCSOL PWO, Athens GA  
NAVSEASYS COM Code 0325, Program Mgr, Washington, DC; Code 05E1, Wash, DC; Code PMS 395 A 3,  
Washington, DC; SEA 04E (L Kess) Washington, DC; SEA05E1, Washington, D.C.  
NAVSECGRUACT Facil. Off., Galeta Is. Panama Canal; PWO, Adak AK; PWO, Edzell Scotland; PWO,  
Puerto Rico; PWO, Torri Sta, Okinawa  
NAVSECSTA PWD - Engr Div, Wash., DC  
NAVSHIPREPFAF SCE Subic Bay  
NAVSHIPYD Bremerton, WA (Carr Inlet Acoustic Range); Code 134, Pearl Harbor, HI; Code 202.4, Long  
Beach CA; Code 202.5 (Library) Puget Sound, Bremerton WA; Code 380, Portsmouth, VA; Code 382.3,  
Pearl Harbor, HI; Code 400, Puget Sound; Code 440 Portsmouth NH; Code 440, Norfolk; Code 440, Puget  
Sound, Bremerton WA; Code 453 (Util. Supr), Vallejo CA; Commander, Philadelphia, PA; L.D. Vivian;  
Library, Portsmouth NH; PW Dept, Long Beach, CA; PWD (Code 420) Dir Portsmouth, VA; PWD (Code  
450-HD) Portsmouth, VA; PWD (Code 453-HD) SHPO 03, Portsmouth, VA; PWD (Code 457-HD) Shop  
07, Portsmouth, VA; PWD (Code 460) Portsmouth, VA; PWO, Bremerton, WA; PWO, Mare Is.; PWO,  
Puget Sound; SCE, Pearl Harbor HI; Tech Library, Vallejo, CA  
NAVSTA Adak, AK; CO Roosevelt Roads P.R. Puerto Rico; CO, Brooklyn NY; Code 4, 12 Marine Corps  
Dist, Treasure Is., San Francisco CA; Dir Engr Div, PWD, Mayport FL; Dir Mech Engr 37WC93 Norfolk,  
VA; Engr. Dir., Rota Spain; Long Beach, CA; Maint. Cont. Div., Guantanamo Bay Cuba; Maint. Div.  
Dir/Code 531, Rodman Panama Canal; PWD (LTG.P.M. Motolenich), Puerto Rico; PWD - Engr Dept,  
Adak, AK; PWD - Engr Div, Midway Is.; PWO, Guantanamo Bay Cuba; PWO, Keflavik Iceland; PWO,  
Mayport FL  
NAVFACENGCOM CONTRACTS ROICC Rota Spain  
NAVSTA SCE, Guam; SCE, Pearl Harbor HI; SCE, San Diego CA; SCE, Subic Bay, R.P.; Utilities Engr Off.  
Rota Spain  
NAVSUBASE Code 23 (Slowey) Bremerton, WA; ENS S. Dove, Groton, CT  
NAVSUPPACT CO, Naples, Italy; PWO Naples Italy  
NAVSUPPFAC PWD - Maint. Control Div, Thurmont, MD  
NAVSURFWPNCCEN PWO, White Oak, Silver Spring, MD  
NAVTECHTRACEN SCE, Pensacola FL  
NAVTELCOMM COM Code 53, Washington, DC  
NAVWPNCEN Code 2636 China Lake; Code 3803 China Lake, CA; PWO (Code 266) China Lake, CA; ROICC  
(Code 702), China Lake CA

NAVWPNSTA (Clebak) Colts Neck, NJ; Code 092, Colts Neck NJ; Code 092, Concord CA; Code 092A, Seal Beach, CA; Maint. Control Dir., Yorktown VA  
NAVWPNSTA PW Office Yorktown, VA  
NAVWPNSTA PWD - Maint. Control Div., Concord, CA; PWD - Supr Gen Engr, Seal Beach, CA; PWO, Charleston, SC; PWO, Seal Beach CA  
NAVWPNSUPPCEN Code 09 Crane IN  
NCBU 405 OIC, San Diego, CA  
NCTC Const. Elec. School, Port Hueneme, CA  
NCBC Code 10 Davisville, RI; Code 15, Port Hueneme CA; Code 155, Port Hueneme CA; Code 156, Port Hueneme, CA; Code 25111 Port Hueneme, CA; Code 400, Gulfport MS; Code 430 (PW Engrng) Gulfport, MS; Code 470.2, Gulfport, MS; NEESA Code 252 (P Winters) Port Hueneme, CA; PWO (Code 80) Port Hueneme, CA; PWO, Davisville RI; PWO, Gulfport, MS  
NCBU 411 OIC, Norfolk VA  
NCR 20, Code R70; 20, Commander  
NMCB 74, CO; FIVE, Operations Dept; Forty, CO; THREE, Operations Off.  
NOAA (Dr. T. Mc Guinness) Rockville, MD; Library Rockville, MD  
NORDA Code 440 (Ocean Rsch Off) Bay St. Louis MS  
NRL Code 5800 Washington, DC; Code 8441 (R.A. Skop), Washington DC  
NROTC J.W. Stephenson, UC, Berkeley, CA  
NSC Code 54.1 Norfolk, VA  
NSD SCE, Subic Bay, R.P.  
NSWSES Code 0150 Port Hueneme, CA  
NTC OICC, CBU-401, Great Lakes IL  
NUSC Code 131 New London, CT; Code 5202 (S. Schady) New London, CT; Code EA123 (R.S. Munn), New London CT; Code SB 331 (Brown), Newport RI; Code TA131 (G. De la Cruz), New London CT  
OFFICE SECRETARY OF DEFENSE OASD (MRA&L) Dir. of Energy, Pentagon, Washington, DC  
ONR Central Regional Office, Boston, MA; Code 221, Arlington VA; Code 485 (Silva) Arlington, VA; Code 700F Arlington VA  
PACMISRANFAC HI Area Bkg Sands, PWO Kekaha, Kauai, HI  
PHIBCB 1 P&E, San Diego, CA; 1, CSWC D Wellington, San Diego, CA  
PMTC Pat. Counsel, Point Mugu CA  
PWC CO Norfolk, VA; CO, (Code 10), Oakland, CA; CO, Great Lakes IL; CO, Pearl Harbor HI; Code 10, Great Lakes, IL; Code 105 Oakland, CA; Code 110, Great Lakes, IL; Code 110, Oakland, CA; Code 120, Oakland CA; Code 120C, (Library) San Diego, CA; Code 128, Guam; Code 154, Great Lakes, IL; Code 200, Great Lakes IL; Code 200, Guam; Code 400, Great Lakes, IL; Commanding Officer, Subic Bay; Code 400, Pearl Harbor, HI; Code 400, San Diego, CA; Code 420, Great Lakes, IL; Code 420, Oakland, CA; Code 424, Norfolk, VA; Code 500 Norfolk, VA; Code 505A Oakland, CA; Code 600, Great Lakes, IL; Code 610, San Diego Ca; Code 700, Great Lakes, IL; Code 700, San Diego, CA; Library, Pensacola, FL; Library, Guam; Library, Norfolk, VA; Library, Oakland, CA; Library, Pearl Harbor, HI; Library, Subic Bay, R.P.; Util Dept (R Pascua) Pearl Harbor, HI; Utilities Officer, Guam  
SPCC PWO (Code 120) Mechanicsburg PA  
SUPANX PWO, Williamsburg VA  
TVA Smelser, Knoxville, Tenn.; Solar Group, Arnold, Knoxville, TN  
UCT ONE OIC, Norfolk, VA  
UCT TWO OIC, Port Hueneme CA  
U.S. MERCHANT MARINE ACADEMY Kings Point, NY (Reprint Custodian)  
USAF REGIONAL HOSPITAL Fairchild AFB, WA  
USAF SCHOOL OF AEROSPACE MEDICINE Hyperbaric Medicine Div, Brooks AFB, TX  
USCG (Smith), Washington, DC; G-EOE-4 (T Dowd), Washington, DC; G-MMT-4/82 (J Spencer)  
USDA Forest Products Lab, Madison WI; Forest Service Reg 3 (R. Brown) Albuquerque, NM; Forest Service, Bowers, Atlanta, GA  
USNA Ch. Mech. Engr. Dept Annapolis MD; Civil Engr Dept (R. Erchyl) Annapolis MD; ENGRNG Div, PWD, Annapolis MD; Energy-Environ Study Grp, Annapolis, MD; Environ. Prot. R&D Prog. (J. Williams), Annapolis MD; Mech. Engr. Dept. (C. Wu), Annapolis MD; NAVSYSENGR Dept, Annapolis, MD; PWO Annapolis MD  
USS FULTON WPNS Rep. Offr (W-3) New York, NY  
WATER & POWER RESOURCES SERVICE (Smaak) Denver, CO  
AMERICAN CONCRETE INSTITUTE Detroit MI (Library)  
ARIZONA Kroelinger Tempe, AZ; State Energy Programs Off., Phoenix AZ  
AUBURN UNIV. Bldg Sci Dept, Lechner, Auburn, AL  
BERKELEY PW Engr Div, Harrison, Berkeley, CA  
BONNEVILLE POWER ADMIN Portland OR (Energy Consrv. Off., D. Davey)  
BROOKHAVEN NATL LAB M. Steinberg, Upton NY  
CALIF. DEPT OF NAVIGATION & OCEAN DEV. Sacramento, CA (G. Armstrong)  
CALIF. MARITIME ACADEMY Vallejo, CA (Library)

CALIFORNIA STATE UNIVERSITY LONG BEACH, CA (CHELAPATI)  
CLARKSON COLL OF TECH G. Batson, Potsdam NY  
CORNELL UNIVERSITY Ithaca NY (Serials Dept, Engr Lib.); Ithaca, NY (Civil & Environ. Engr)  
DAMES & MOORE LIBRARY LOS ANGELES, CA  
DRURY COLLEGE Physics Dept, Springfield, MO  
DUKE UNIV MEDICAL CENTER B. Muga, Durham NC  
UNIVERSITY OF DELAWARE (Dr. S. Dexter) Lewes, DE  
FLORIDA ATLANTIC UNIVERSITY Boca Raton FL (W. Hartt); Boca Raton, FL (McAllister)  
FOREST INST. FOR OCEAN & MOUNTAIN Carson City NV (Studies - Library)  
GEORGIA INSTITUTE OF TECHNOLOGY (LT R. Johnson) Atlanta, GA; Col. Arch, Benton, Atlanta, GA  
HARVARD UNIV. Dept. of Architecture, Dr. Kim, Cambridge, MA  
HAWAII STATE DEPT OF PLAN. & ECON DEV. Honolulu HI (Tech Info Ctr)  
INSTITUTE OF MARINE SCIENCES Morehead City NC (Director)  
IOWA STATE UNIVERSITY Dept. Arch, McKown, Ames, IA  
WOODS HOLE OCEANOGRAPHIC INST. Woods Hole MA (Winget)  
KEENE STATE COLLEGE Keene NH (Cunningham)  
LEHIGH UNIVERSITY BETHLEHEM, PA (MARINE GEOTECHNICAL LAB., RICHARDS); Bethlehem  
PA (Linderman Lib. No.30, Flecksteiner)  
LOUISIANA DIV NATURAL RESOURCES & ENERGY Div Of R&D, Baton Rouge, LA  
MAINE MARITIME ACADEMY CASTINE, ME (LIBRARY)  
MAINE OFFICE OF ENERGY RESOURCES Augusta, ME  
MICHIGAN TECHNOLOGICAL UNIVERSITY Houghton, MI (Haas)  
MISSOURI ENERGY AGENCY Jefferson City MO  
MIT Cambridge MA; Cambridge MA (Rm 10-500, Tech. Reports, Engr. Lib.); Cambridge, MA (Harleman)  
MONTANA ENERGY OFFICE Anderson, Helena, MT  
NATURAL ENERGY LAB Library, Honolulu, HI  
NEW HAMPSHIRE Concord NH (Governor's Council on Energy)  
NEW MEXICO SOLAR ENERGY INST. Dr. Zwibel Las Cruces NM  
NY CITY COMMUNITY COLLEGE BROOKLYN, NY (LIBRARY)  
NYS ENERGY OFFICE Library, Albany NY  
OAK RIDGE NATL LAB T. Lundy, Oak Ridge, TN  
OREGON STATE UNIVERSITY (CE Dept Grace) Corvallis, OR; CORVALLIS, OR (CE DEPT, HICKS);  
Corvallis OR (School of Oceanography)  
PENNSYLVANIA STATE UNIVERSITY STATE COLLEGE, PA (SNYDER)  
POLLUTION ABATEMENT ASSOC. Graham  
PURDUE UNIVERSITY Lafayette, IN (CE Engr. Lib)  
CONNECTICUT Hartford CT (Dept of Plan. & Energy Policy)  
SAN DIEGO STATE UNIV. 1. Noorany San Diego, CA  
SCRIPPS INSTITUTE OF OCEANOGRAPHY LA JOLLA, CA (ADAMS); San Diego, CA (Marina Phy. Lab.  
Spieess)  
SEATTLE U Prof Schwaegler Seattle WA  
SRI INTL Phillips, Chem Engr Lab, Menlo Park, CA  
STATE UNIV. OF NEW YORK Buffalo, NY; Fort Schuyler, NY (Longobardi)  
STATE UNIV. OF NY AT BUFFALO School of Medicine, Buffalo, NY  
TEXAS A&M UNIVERSITY College Station TX (CE Dept. Herbich); W.B. Ledbetter College Station, TX  
UNIVERSITY OF CALIFORNIA BERKELEY, CA (CE DEPT, GERWICK); Berkeley CA (E. Pearson);  
DAVIS, CA (CE DEPT, TAYLOR); Energy Engineer, Davis CA; LIVERMORE, CA (LAWRENCE  
LIVERMORE LAB, TOKARZ); UCSF, Physical Plant, San Francisco, CA  
UNIVERSITY OF DELAWARE Newark, DE (Dept of Civil Engineering, Chesson)  
UNIVERSITY OF FLORIDA Dept Arch., Morgan, Gainesville, FL  
UNIVERSITY OF HAWAII HONOLULU, HI (SCIENCE AND TECH. DIV.)  
UNIVERSITY OF ILLINOIS (Hall) Urbana, IL; Metz Ref Rm, Urbana IL; URBANA, IL (DAVISON);  
URBANA, IL (LIBRARY); Urbana IL (CE Dept, W. Gamble)  
UNIVERSITY OF MASSACHUSETTS (Heronemus), ME Dept, Amherst, MA  
UNIVERSITY OF NEBRASKA-LINCOLN Lincoln, NE (Ross Ice Shelf Proj.)  
UNIVERSITY OF NEW HAMPSHIRE Elec. Engr. Depot, Dr. Murdoch, Durham, N.H.  
UNIVERSITY OF PENNSYLVANIA PHILADELPHIA, PA (SCHOOL OF ENGR & APPLIED SCIENCE,  
ROLL)  
UNIVERSITY OF TEXAS Inst. Marine Sci (Library), Port Arkansas TX  
UNIVERSITY OF TEXAS AT AUSTIN AUSTIN, TX (THOMPSON); Austin, TX (Breen)  
UNIVERSITY OF WASHINGTON Dept of Civil Engr (Dr. Mattock). Seattle WA; SEATTLE, WA (OCEAN  
ENG RSCH LAB, GRAY); Seattle WA (E. Linger)  
UNIVERSITY OF WISCONSIN Milwaukee WI (Ctr of Great Lakes Studies)  
VENTURA COUNTY PWA (Brownie) Ventura, CA  
WESTERN ARCHEOLOGICAL CENTER Library, Tucson AZ

ALFRED A. YEE & ASSOC. Librarian, Honolulu, HI  
AMETEK Offshore Res. & Engr Div  
ARVID GRANT OLYMPIA, WA  
ATLANTIC RICHFIELD CO. DALLAS, TX (SMITH)  
BECHTEL CORP. SAN FRANCISCO, CA (PHELPS)  
BROWN & ROOT Houston TX (D. Ward)  
CHEMED CORP Lake Zurich IL (Dearborn Chem. Div.Lib.)  
COLUMBIA GULF TRANSMISSION CO. HOUSTON, TX (ENG. LIB.)  
CONTINENTAL OIL CO O. Maxson, Ponca City, OK  
DESIGN SERVICES Beck, Ventura, CA  
DILLINGHAM PRECAST F. McHale, Honolulu HI  
DIXIE DIVING CENTER Decatur, GA  
DRAVO CORP Pittsburgh PA (Wright)  
DURLACH, O'NEAL, JENKINS & ASSOC. Columbia SC  
EVALUATION ASSOC. INC KING OF PRUSSIA, PA (FEDELE)  
EXXON PRODUCTION RESEARCH CO Houston, TX (Chao)  
FORD, BACON & DAVIS, INC. New York (Library)  
FURGO INC. Library, Houston, TX  
GARD INC. Dr. L. Holmes, Niles, IL  
GENERAL DYNAMICS Elec. Boat Div., Environ. Engr (H. Wallman), Groton CT  
GEOTECHNICAL ENGINEERS INC. Winchester, MA (Paudling)  
GLIDDEN CO. STRONGSVILLE, OH (RSCH LIB)  
GOULD INC. Tech Lib, Ches Instru Div Glen Burnie MD  
HALEY & ALDRICH, INC. Cambridge MA (Aldrich, Jr.)  
NUSC Library, Newport, RI  
KENNETH TATOR ASSOC CORAOPOLIS, PA (LIBRARY)  
LIN OFFSHORE ENGRG P. Chow, San Francisco CA  
LOCKHEED MISSILES & SPACE CO. INC. Dept 57-22 (Rynewicz) Sunnyvale, CA  
MARATHON OIL CO Houston TX  
MARINE CONCRETE STRUCTURES INC. MEFAIRIE, LA (INGRAHAM)  
MCDONNEL AIRCRAFT CO. (Fayman) Support Tech Dept St. Louis, MO  
MEDERMOTT & CO. Diving Division, Harvey, LA  
MOBIL PIPE LINE CO. DALLAS, TX MGR OF ENGR (NOACK)  
MOFFATT & NICHOL ENGINEERS (R. Palmer) Long Beach, CA  
MUESER, RUTLEDGE, WENTWORTH AND JOHNSTON New York (Richards)  
NEWPORT NEWS SHIPBLDG & DRYDOCK CO. Newport News VA (Tech. Lib.)  
PACIFIC MARINE TECHNOLOGY (M. Wagner) Duvall, WA  
PG&E Library, San Francisco, CA  
PORTLAND CEMENT ASSOC. SKOKIE, IL (CORLEY; SKOKIE, IL (KLIEGER); Skokie IL (Rsch & Dev  
Lab, Lib.))  
RAYMOND INTERNATIONAL INC. E Colle Soil Tech Dept. Pennsauken, NJ; J. Welsh Soiltech Dept.  
Pennsauken, NJ  
SANDIA LABORATORIES Albuquerque, NM (Vortman); Library Div., Livermore CA  
SCHUPACK ASSOC SO. NORWALK, CT (SCHUPACK)  
SEAFOOD LABORATORY MOREHEAD CITY, NC (LIBRARY)  
SEATECH CORP. MIAMI, FL (PERONI)  
SHELL DEVELOPMENT CO. Houston TX (C. Sellars Jr.)  
SHELL OIL CO. HOUSTON, TX (MARSHALL)  
TECHNICAL COATINGS CO Oakmont PA (Library)  
TEXTRON INC BUFFALO, NY (RESEARCH CENTER LIB.)  
TIDEWATER CONSTR. CO Norfolk VA (Fowler)  
TRW SYSTEMS REDONDO BEACH, CA (DAI)  
UNION CARBIDE CORP. R.J. Martell Boston, MA  
UNITED TECHNOLOGIES Windsor Locks CT (Hamilton Std Div., Library)  
WARD, WOLSTENHOLD ARCHITECTS Sacramento, CA  
WESTINGHOUSE ELECTRIC CORP. Annapolis MD (Oceanic Div Lib, Bryan); Library, Pittsburgh PA  
WISS, JANNEY, ELSTNER, & ASSOC Northbrook, IL (D.W. Pfeifer)  
WM CLAPP LABS - BATTELLE DUXBURY, MA (LIBRARY)  
WOODWARD-CLYDE CONSULTANTS PLYMOUTH MEETING PA (CROSS, III)  
BRAHTZ La Jolla, CA  
BULLOCK La Canada  
DOBROWOLSKI, J.A. Altadena, CA  
ERVIN, DOUG Belmont, CA  
FISHER San Diego, Ca  
GERWICK, BEN C. JR San Francisco, CA

KETRON, BOB Ft Worth, TX  
KRUZIC, T.P. Silver Spring, MD  
LAFKIN Seattle, WA  
LAYTON Redmond, WA  
PAULI Silver Spring, MD  
R.F. BESIER Old Saybrook CT  
BROWN & CALDWELL Saunders, E.M./Oakland, CA  
SMITH Gulfport, MS  
T.W. MERMEL Washington DC  
WALTZ Livermore, CA